

DEPARTMENT OF ECONOMICS, MANAGEMENT AND STATISTICS

UNIVERSITY OF MILAN – BICOCCA

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# Factor Vector Autoregressive Estimation of Heteroskedastic Persistent and Non Persistent Processes Subject to Structural Breaks

Claudio Morana No. 273 – May 2014

Dipartimento di Economia, Metodi Quantitativi e Strategie di Impresa Università degli Studi di Milano - Bicocca <u>http://dems.unimib.it/</u>

# Factor Vector Autoregressive Estimation of Heteroskedastic Persistent and Non Persistent Processes Subject to Structural Breaks

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First draft December 2010; this draft 28 May 2014

#### Abstract

In the paper a general framework for large scale modeling of macroeconomic and financial time series is introduced. The proposed approach is characterized by simplicity of implementation, performing well independently of persistence and heteroskedasticity properties, accounting for common deterministic and stochastic factors. Monte Carlo results strongly support the proposed methodology, validating its use also for relatively small cross-sectional and temporal samples.

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<sup>&</sup>lt;sup>†</sup>A previous version of the paper was presented at the 19th and 21st Annual Symposium of the Society for Non Linear Dynamics and Econometrics, the 4th and 6th Annual Conference of the Society for Financial Econometrics, the 65th European Meeting of the Econometric Society (ESEM), the 2011 NBER-NSF Time Series Conference, the 5th CSDA International Conference on Computational and Financial Econometrics. The author is grateful to conference participants, N. Cassola, F.C. Bagliano, C. Conrad, R.T. Baillie and J. Bai for constructive comments. This project has received funding from the European Union's Seventh Framework Programme for research, technological development and demonstration under grant agreement no. 3202782013-2015, and PRIN-MIUR 2009.

<sup>&</sup>lt;sup>‡</sup>As Mitsuo Aida wrote in one of his poems, somewhere in life/ there is a path/ that must be taken regardless of how hard we try to avoid it/ at that time, all one can do is remain silent and walk the path/ neither complaining nor whining/ saying nothing and walking on/ just saying nothing and showing no tears/ it is then,/ as human beings,/ that the roots of our souls grow deeper. This paper is dedicated to the loving memory of A.

#### JEL classification: C22 $\,$

*Key words*: long and short memory, structural breaks, common factors, principal components analysis, fractionally integrated heteroskedastic factor vector autoregressive model.

### 1 Introduction

In the paper a general strategy for large-scale modeling of macroeconomic and financial data, set within the factor vector autoregressive model (F-VAR) framework, is proposed.<sup>1</sup>

Following the lead of dynamic factor model analysis proposed in Geweke (1977), it is assumed that a small number of structural shocks are responsible for the observed comovement in economic data; it is however also assumed that commonalities across series are described by deterministic factors, i.e., common break processes. Comovement across series is then accounted by both deterministic and stochastic factors; moreover, common factors are allowed in both mean and variance, covering the I(0) and I(1) persistence cases, as well as the intermediate case of long memory, i.e., I(d), 0 < d < 1. As the common factors are unobserved, accurate estimation may fail in the framework of small scale vector autoregressive (VAR) models, but succeed when cross-sectional information is employed to disentangle common and idiosyncratic features.

The proposed fractionally integrated heteroskedastic factor vector autoregressive model (FI-HF-VAR) bridges the F-VAR and (the most recent) G-VAR literature, as, similarly to Dees et al. (2010) and Pesaran and Smith (2011), a weakly stationary cyclical representation is employed; yet, similarly to Bai and Ng (2004) principal components analysis (PCA) is employed for the estimation of the latent factors. Consistent and asymptotically normal estimation is performed by means of QML, also implemented through an iterative multi-step estimation procedure. Monte Carlo results strongly support the proposed methodology.

Overall, the FI-HF-VAR model can be understood as a unified framework for large-scale econometric modeling, allowing for accurate investigation of cross-sectional and time series features, independent of persistence and heteroskedasticity properties of the data, from comovement to impulse responses, forecast error variance and historical decomposition analysis.

After this introduction, the paper is organized as follows. In Section 2 the econometric model is presented, in Section 3 estimation is discussed, while Monte Carlo analysis is performed in Section 4; finally, conclusions are drawn in Section 5.

<sup>&</sup>lt;sup>1</sup>The literature on F-VAR models is large. See Stock and Watson (2011) for a survey.

### 2 The FI-HF-VAR model

Consider the following fractionally integrated heteroskedastic factor vector autoregressive (FI-HF-VAR) model

$$x_t - \Lambda_{\mu} \mu_t - \Lambda_f f_t = C(L)(x_{t-1} - \Lambda_{\mu} \mu_{t-1} - \Lambda_f f_{t-1}) + v_t$$

$$v_t \sim i.i.d.(0, \Sigma_v)$$
(1)

$$P(L)D(L)f_t = \eta_t = H_t^{1/2}\psi_t \qquad (2)$$
  
$$\psi_t \sim i.i.d.(0, I_R),$$

where  $x_t$  is a  $N \times 1$  vector of real valued integrated and heteroskedastic processes subject to structural breaks, t = 1, ..., T, in deviation from the unobserved common deterministic  $(\mu_t)$  and stochastic  $(f_t)$  factors;  $C(L) \equiv$  $C_0L^0 + C_1L + C_2L^2 + ... + C_sL^s$  is a finite order matrix of polynomials in the lag operator with all the roots outside the unit circle,  $C_j$ , j = 0, ..., s, is a square matrix of coefficients of order N;  $v_t$  is a  $N \times 1$  vector of zero mean idiosyncratic i.i.d. shocks, with contemporaneous covariance matrix  $\Sigma_v$ , assumed to be coherent with the condition of weak cross-sectional correlation of the idiosyncratic components (Assumption E) stated in Bai (2003, p.143). The model in (1) actually admits the same static representation of Bai (2003), as it can be rewritten as  $x_t = \Lambda_{\mu}\mu_t + \Lambda_f f_t + [I - C(L)]^{-1} v_t$ .

### 2.1 The common break process component

The vector of common break processes  $\mu_t$  is  $M \times 1$ , with  $M \leq N$ , and  $N \times M$  matrix of loadings  $\Lambda_{\mu}$ ; the latter are assumed to be orthogonal to the common stochastic factors  $f_t$ , and of unknown form, measuring recurrent or non recurrent changes in mean, with smooth or abrupt transition across regimes; the generic element in  $\mu_t$  is  $\mu_{i,t} \equiv z_{\mu,i}(t)$ , where  $z_{\mu,i}(t)$ , i = 1, ..., M, is a function of the time index t, t = 1, ..., T.

The idiosyncratic break process  $z_{\mu,i}(t)$  can take different forms. For instance, Bai and Perron (1998) use a discontinuous function,

$$z_{\mu,i}(t) = \delta_{i,0} + \sum_{j=1}^{J} \delta_{i,j} I_{\tau_j},$$
(3)

where  $I_{\tau_j}$  is the indicator function, such that  $I_{\tau_j} = 1$  if  $t > \tau_j$  and is 0 otherwise; in Bai and Perron (1998) the break points  $\tau_j$  are determined through testing; a Markov switching mechanism, as in Hamilton (1989), could however also be employed to this purpose.

Differently, Enders and Lee (2012) and Baillie and Morana (2009, 2012) model the break process as a continuous and bounded function of time, by means of a Fourier expansion (Gallant, 1984), i.e.,

$$z_{\mu,i}(t) = \delta_{i,0} + \sum_{j=1}^{J} \delta_{i,s,j} \sin(2\pi j t/T) + \delta_{i,c,j} \cos(2\pi j t/T), \quad j \le T/2.$$
(4)

Similarly Gonzalez and Terasvirta (2008), using a logistic specification

$$z_{\mu,i}(t) = \delta_{i,0} + \sum_{j=1}^{J} \delta_{i,j} g(\eta_{j,} c_{j}, t^{*}), \qquad (5)$$

where the logistic function is  $g(\eta_j, c_j, t^*) = (1 + \exp(-\gamma(\eta)(t^* - c_j)/\hat{\sigma}_{t^*}))^{-1}$ ,  $\gamma(\eta) = \exp(\eta_j), c_j \in [0, 1]$  and  $\eta_j$  are parameters,  $t^* = t/T$ , and  $\hat{\sigma}_{t^*}$  is the estimated standard deviation of  $t^*$ . In particular, as  $\eta_j \to \infty, g(\cdot)$  becomes the indicator function, yielding therefore a generalization of the Bai-Perron specification.

Also similarly Engle and Rangle (2008) and Beran and Weiershauser (2011), using a spline function

$$z_{\mu,i}(t) = S(\frac{t}{T}),\tag{6}$$

where  $S(\frac{t}{T}) = \sum_{j=1}^{p+2} a_j f_j(\frac{t}{T})$  is a spline function of order p,  $a_j$  are unknown regression coefficients and the functions  $f_j(\cdot)$  are spline basis functions defined as  $f_1 = 1, f_2 = (\frac{t}{T}), ..., f_{p+1} = (\frac{t}{T})^p$ , and  $f_{p+2} = (\frac{t}{T} - \eta)^p$  with  $\eta \in (\frac{1}{T}, 1)$ .

A semiparametric approach has also been suggested by Beran and Feng (2002a), using a kernel function, i.e.,

$$z_{\mu,i}(t) = \frac{1}{Tb} \sum_{j=1}^{T} K(\frac{t-t_j}{b}) x_{i,j},$$
(7)

where b is the bandwidth and  $K(\cdot)$  is the kernel function, specified as  $K(u) = \sum_{l=0}^{r} \alpha_l u^{2l}$  for  $|u| \le 1$  and K(u) = 0 for |u| > 1; r = 0, 1, 2, ..., and the coefficient  $\alpha_l$  are such that  $\int_{-1}^{1} K(u) du = 1$ .

Finally, a random level shift model has been proposed by Engle and Smith (1999), Ray and Tsay (2002), Lu and Perron (2010) and Perron and Varneskov (2012); for instance, Perron and Varneskov (2012) define the break process as

$$z_{\mu,i}(t) = \sum_{j=1}^{T} \delta_{T,i,j},$$
(8)

where  $\delta_{T,i,j} = \pi_{T,t}\eta_t$ ,  $\eta_t \sim i.i.d.N(0,\sigma^2)$  and  $\pi_{T,t} \sim i.i.d.Bernoulli(p/T,1)$  for  $p \ge 0$ .

In the case M = N there are no common break processes, i.e., each series is characterized by its own idiosyncratic break process and the  $N \times M$ factor loading matrix  $\Lambda_{\mu}$  is square, diagonal and of full rank; when M < N, then there exist M common break processes and the factor loading matrix is of reduced rank (M). Hence, in the latter case the series  $x_t$  may be said cotrending, according to Chapman and Ogaki (1993), nonlinear cotrending, according to Bierens (2000), or cobreaking, according to Hendry (1996) and Hendry and Massmann (2007). The representation in (1) emphasizes however the driving role of the common break processes, rather than the break-free linear combinations (cobreaking/cotrending relationships) relating the series  $x_t$ .

#### 2.2 The common break-free component

The vector of (zero-mean) integrated heteroskedastic common factors  $f_t$  is  $R \times 1$ , with  $R \leq N$ , and  $N \times R$  matrix of loadings  $\Lambda_f$ . The order of integration is  $d_i$  in mean, and  $b_i$  in variance,  $0 \leq d_i \leq 1, 0 \leq b_i \leq 1, i = 1, ..., R$ .

The polynomial matrix  $P(L) \equiv I_R - P_1L - P_2L^2 - ... - P_uL^u$  is of finite order, with all the roots outside the unit circle;  $P_j$ , j = 1, ..., u, is a square matrix of coefficients of order R;  $\psi_t$  is a  $R \times 1$  vector of common zero mean i.i.d. shocks, with identity covariance matrix  $I_R$ ,  $E[\psi_{it}v_{js}] = 0$  all i, j, t, s, respectively.

The matrix D(L) is a  $R \times R$  diagonal matrix in the lag operator, specified according to the integration order (in mean) of the common stochastic factors, i.e.,

$$D(L) \equiv (1-L)I_R,$$

for the case of I(1) integration  $(d_i = 1)$ ;

$$D(L) \equiv I_R$$

for the I(0) or no integration (short memory) case  $(d_i = 0)$ ;

$$D(L) \equiv diag \left\{ (1-L)^{d_1}, (1-L)^{d_2}, ..., (1-L)^{d_R} \right\},\$$

for the case of fractional integration (I(d), long memory)  $(0 < d_i < 1)$ , where  $(1-L)^{d_i}$  is the fractional differencing operator; the latter admits a binomial expansion, which can be compactly written in terms of the Hypergeometric function, i.e.,

$$(1-L)^{d_i} = F(-d_i, 1, 1; L)$$
  
=  $\sum_{k=0}^{\infty} \Gamma(k-d_i) \Gamma(k+1)^{-1} \Gamma(-d_i)^{-1} L^k$   
=  $\sum_{k=0}^{\infty} \pi_k L^k$ , (9)

where  $\Gamma(\cdot)$  is the Gamma function.<sup>2</sup>

In the case R = N there are no common stochastic processes, i.e., each series is characterized by its own idiosyncratic persistent stochastic component, and the  $N \times R$  factor loading matrix  $\Lambda_f$  is square, diagonal and of full rank; when R < N, then there exist R common stochastic processes and the factor loading matrix is of reduced rank (R). Hence, in the latter case the series  $x_t$  show common stochastic features, according to Engle and Kozicki (1993). The concept of common feature is broad, encompassing the notion of cointegration and fractional cointegration (Engle and Granger, 1987; Johansen, 2011), holding for the  $0 < d_i \leq 1$  case. The representation in (1) emphasizes however the driving role of the common stochastic factors rather than the feature-free linear combinations (cofeature relationships) relating the series  $x_t$ .

#### 2.3 The conditional variance process

The  $R \times R$  conditional variance-covariance matrix for the unconditionally and conditionally orthogonal common factors  $f_t$  is  $H_t = Var(f_t | \Omega_{t-1}) \equiv$  $diag\{h_{1,t}, h_{2,t}, ..., h_{R,t}\}$ , where  $\Omega_{t-1}$  is the information set available at time period t-1. Consistent with the constant conditional correlation model of Bollerslev (1990) and Brunetti and Gilbert (2000), the *i*th generic element along the main diagonal of  $H_t$  is

$$m_i(L)h_{i,t} = w_{i,t} + n_i(L)\eta_{i,t}^2, \qquad i = 1, ..., R,$$
(10)

where

$$n_i(L) \equiv 1 - \beta_i(L) - (1 - \varphi_i(L))(1 - L)^{b_i}$$
(11)

<sup>&</sup>lt;sup>2</sup>See Baillie (1996) for an introduction to long memory processes.

for the case of fractional integration (long memory) in variance  $(0 < b_i < 1)$ ;

$$n_i(L) \equiv 1 - \beta_i(L) - (1 - \varphi_i(L))(1 - L)$$
(12)

for the case of I(1) integration in variance  $(b_i = 1)$ ;

$$n_i(L) \equiv 1 - \beta_i(L) - (1 - \varphi_i(L)) \tag{13}$$

for the I(0) or no integration (short memory) in variance case  $(b_i = 0)$ ; in all cases

$$m_i(L) \equiv 1 - \beta_i(L) \tag{14}$$

$$\varphi_i(L) = \alpha_i(L) + \beta_i(L) \tag{15}$$

$$\alpha_i(L) \equiv \alpha_{i,1}L + \alpha_{i,2}L^2 + \dots + \alpha_{i,q}L^q \tag{16}$$

$$\beta_i(L) \equiv \beta_{i,1}L + \beta_{i,2}L^2 + \dots + \beta_{i,p}L^p, \tag{17}$$

and all the roots of the  $\alpha_i(L)$  and  $\beta_i(L)$  polynomials are outside the unit circle.

The conditional variance process  $h_{i,t} \equiv Var(f_{i,t}|\Omega_{i,t-1})$ , i = 1, ..., R, is therefore of the *FIGARCH*  $(p, b_i, z)$  type (Baillie et al., 1996)<sup>3</sup>, with  $z = max \{p, q\}$ , or the *IGARCH* (p, q) type (Engle and Bollerslev, 1986), for the fractionally integrated and integrated case, respectively; of the *GARCH* (p, q)type (Bollerslev, 1986) for the non integrated case. The model is however not standard as the intercept component  $w_{i,t}$  is time-varying, allowing for structural breaks in variance; similarly to the mean part of the model, structural breaks in variance are assumed to be of unknown form, measuring recurrent or non recurrent regimes, with smooth or abrupt transition; then,  $w_{i,t} \equiv z_{h,i}(t)$ , where  $z_{h,i}(t)$  is a continuous or discontinuous bounded function of the time index t, t = 1, ..., T, which can be parameterized as in (3), (4), (5), (6), or (7). See Engle and Rangel (2008), Baillie and Morana (2009), Cassola and Morana (2012), Amado and Terasvirta (2008), Hamilton and Susmel (1994) and Beine and Laurent (2000).

The following  $ARCH(\infty)$  representation can be obtained from each of the three above models

$$h_{i,t} = \frac{w_{i,t}}{m_i(1)} + \frac{n_i(L)}{m_i(L)}\eta_{i,t}^2 \qquad i = 1, ..., R$$
(18)

$$= w_{i,t}^* + \psi_i(L)\eta_{i,t}^2, \tag{19}$$

 $<sup>^{3}</sup>$ An alternative long memory specification for the conditional variance process is proposed by Conrad and Karanasos (2006).

where  $w_{i,t}^* = \frac{w_{i,t}}{m_i(1)}$  and  $\psi_i(L) = \frac{n_i(L)}{m_i(L)} = \psi_{1,i}L + \psi_{2,i}L^2 + \dots$ 

The term  $w_{i,t}^{*}$  then bears the interpretation of break in variance process, or time-varying unconditional variance process (no integration case), or long-term conditional variance level (unit root and fractional integration cases).

To guarantee the non negativity of the conditional variance process at each point in time all the coefficients in the  $ARCH(\infty)$  representation must be non-negative, i.e.,  $\psi_{j,i} \ge 0$  for all  $j \ge 1$  and  $w_{i,t}^* > 0$  for any t. Sufficient conditions, for various parameterization, can be found in Baillie et al. (1996), Engle and Bollerslev (1986), Bollerslev (1986), Baillie and Morana (2009), Conrad and Haag (2006), and Chung (1999).

#### 2.4 Examples of nested models

From (1) and (2), by setting  $D(L) = I_R$ ,  $H_t^{1/2} = \Sigma_{\eta}^{1/2}$ , M = N,  $\mu_t = \mu$ ,  $\Lambda_{\mu} = I_N$ , the I(0) homoskedastic F-VAR(*s*, *u*) model

$$x_t - \mu - \Lambda_f f_t = C(L)(x_{t-1} - \mu - \Lambda_f f_{t-1}) + v_t \qquad (20)$$
$$v_t \sim i.i.d.(0, \Sigma_v)$$

$$P(L)f_t = \eta_t, \qquad (21)$$
  
$$\eta_t \sim i.i.d.(0, \Sigma_{\eta})$$

is then obtained; moreover, by allowing  $H_t^{1/2}$  to evolve according to (10), (13), and (14)-(17), with  $w_{i,t} = w_i$ ,  $m_i(L) \equiv 1 - \beta_{i,1}L$  and  $\varphi_i(L) = \alpha_{i,1}L + \beta_{i,1}L$ , the I(0) F-VAR(s, u)-GARCH(1,1) model is obtained; also, by assuming (11) rather then (13), the I(0) F-VAR(s, u)-FIGARCH(1,b,1) is obtained. Applications of the latter models for the modeling of macroeconomic variables in stationary form and financial returns may be envisaged. See, for instance, Morana (2013) and Bagliano and Morana (2014) for large-scale applications to the modeling of the global economy and the macro-finance interface.

Moreover, by setting  $D(L) \equiv (1 - L)I_R$ , the I(1) F-VAR(s, u) model

$$x_{t} - \mu - \Lambda_{f} f_{t} = C(L)(x_{t-1} - \mu - \Lambda_{f} f_{t-1}) + v_{t}$$
(22)  
$$v_{t} \sim i.i.d.(0, \Sigma_{v})$$

$$P(L)(1-L)f_t = \eta_t, \qquad (23)$$
  
$$\eta_t \sim i.i.d.(0, \Sigma_{\eta})$$

is obtained, as well as, by imposing the same restrictions as above, the I(1) F-VAR(s, u)-GARCH(1, 1) and F-VAR(s, u)-FIGARCH(1, b, 1) models. Ap-

plications of the latter models for the modeling of non-stationary macroeconomic variables and financial asset prices may be foreseen.

In addition to interest rate spreads term structure modeling (Morana, 2014; Cassola and Morana, 2012), other applications of the most general framework contributed in the paper may also be envisaged, concerning, for instance, inflation rates and realized moments of financial returns.

#### 2.5 The reduced fractional VAR form

Depending on the persistence properties of the data, the vector autoregressive representation (VAR) for the factors  $f_t$  and the series  $x_t$  can be written as follows.

i) For the case of fractional integration (long memory)  $(0 < d_i < 1)$ , by taking into account the binomial expansion in (9), it follows  $P(L)D(L) \equiv$  $I - \Pi(L)$ ,  $\Pi(L) = \Pi_1 L + \Pi_2 L^2 + ...$ , where  $\Pi_i$ , i = 1, 2, ..., is a square matrix of coefficients of dimension R; by substituting (2) into (1) and rearranging, the infinite order vector autoregressive representation for the factors  $f_t$  and the series  $x_t$  can then be written as

$$\begin{bmatrix} f_t \\ x_t - \Lambda_{\mu}\mu_t \end{bmatrix} = \begin{bmatrix} \Pi_f^*(L) & 0 \\ \Pi^*(L) & C(L) \end{bmatrix} \begin{bmatrix} f_{t-1} \\ x_{t-1} - \Lambda_{\mu}\mu_{t-1} \end{bmatrix}$$
(24)
$$+ \begin{bmatrix} \eta_t \\ \varepsilon_t \end{bmatrix},$$
$$\begin{bmatrix} \eta_t \\ \varepsilon_t \end{bmatrix} = \begin{bmatrix} I \\ \Lambda_f \end{bmatrix} [H_t^{1/2}\psi_t] + \begin{bmatrix} 0 \\ v_t \end{bmatrix},$$

where  $\Pi_f^*(L) = \Pi(L)L^{-1}$  and  $\Pi^*(L) = [\Lambda_f \Pi(L)L^{-1} - C(L)\Lambda_f]$ ; since the infinite order representation cannot be handled in estimation, a truncation to a suitable large lag for the polynomial matrix  $\Pi(L)$  is required.<sup>4</sup> Hence,

$$\Pi(L) \simeq \sum_{j=1}^{p} \Pi_j L^j.$$

<sup>&</sup>lt;sup>4</sup>Monte Carlo evidence reported in Chan and Palma (1998) suggests that the truncation lag should increase with the sample size and the complexity of the ARFIMA representation of the long memory process, still remaining very small relatively to the sample size. For instance, for the covariance stationary fractional white noise case and a sample of 100 observations truncation can be set as low as 6 lags, while for a sample of 10,000 observations it should be increased to 14 lags; for the case of a covariance stationary ARFIMA (1,d,1) process and a sample of 1,000 observations truncation may be set to 30 lags. See Chan and Palma (1998) for further details.

Also for the case of no integration (short memory)  $(d_i = 0)$  and integration  $(d_i = 1)$  the (finite order) vector autoregressive representation for the factors  $f_t$  and the series  $x_t$  can be written as in (24); yet:

*ii*) for the case of no integration (short memory)  $(d_i = 0)$ , recalling that  $D(L) \equiv I_R$ , and therefore P(L)D(L) = P(L), then  $\Pi(L) = P_1L + P_2L^2 + \dots + P_uL^u$ ;

*iii*) for the case of integration  $(d_i = 1)$ , it should be firstly recalled that

$$P(L)D(L) \equiv P(L)(1-L) \tag{25}$$

$$\equiv (I_R - \rho L) - (P_1 L + P_2 L^2 + \dots + P_u L^u)(1 - L) \quad (26)$$

with  $\rho = I_R$ ; the latter may be rewritten in the equivalent polynomial matrix form

$$I_R - \Gamma_1 L - \Gamma_2 L^2 - \dots - \Gamma_{u+1} L^{u+1}$$
(27)

where  $\Gamma_i$ , i = 1, ..., u + 1, is a square matrix of coefficients of dimension R, and

$$\Gamma_1 + \Gamma_2 + \dots + \Gamma_{u+1} = \rho = I_R$$
$$P_i = -(\Gamma_{i+1} + \Gamma_{i+2} + \dots + \Gamma_{u+1}), \quad i = 1, 2, \dots, u;$$

then,  $\Pi(L) = \Gamma_1 L + \Gamma_2 L^2 + \dots + \Gamma_{u+1} L^{u+1}$ .

#### 2.5.1 Reduced form and structural vector moving average representation of the FI-HF-VAR model

In the presence of unconditional heteroskedasticity, the computation of the impulse response functions and the forecast error variance decomposition (FEVD) should be made dependent on the estimated unconditional variance for each regime. In the case of (continuously) time-varying unconditional variance, policy analysis may be then computed at each point in time. For some of the conditional variance models considered in the paper, i.e., the FIGARCH and IGARCH processes, the population unconditional variance does not actually exist; in the latter cases the  $w_{i,t}$  component just bears the interpretation of *long term level* for the conditional variance; policy analysis is still feasible, yet subject to a different interpretation, FEVD referring, for instance, not to the proportion of forecast error (unconditional) variance accounted by each structural shock.

With this caveat in mind, the actual computation of the above quantities is achieved in the same way as in the case of well defined population unconditional variance.

Hence, the computation of the vector moving average (VMA) representation for the FI-HF-VAR model depends on the persistence properties of the data. The following distinctions should then be made.

For the short memory case, i.e., the zero integration order case  $(d_i = 0)$ , the VMA representation for the factors  $f_t$  and the  $x_t - \Lambda_{\mu}\mu_t$  gap series can be written as

$$\begin{bmatrix} f_t \\ x_t - \Lambda_\mu \mu_t \end{bmatrix} = \begin{bmatrix} U(L) & 0 \\ G(L) & F(L) \end{bmatrix} \begin{bmatrix} \eta_t \\ v_t \end{bmatrix},$$
 (28)

where  $U(L) \equiv P(L)^{-1}$ ,  $G(L) \equiv \Lambda_f P(L)^{-1}$  and  $F(L) \equiv [I - C(L)L]^{-1}$ .

For the long memory case  $(0 < d_i < 1)$  and the case of I(1) non stationarity  $(d_i = 1)$ , the VMA representation should be computed for the differenced process yielding

$$(1-L)\begin{bmatrix} f_t\\ x_t - \Lambda_{\mu}\mu_t \end{bmatrix} = \begin{bmatrix} U(L)^+ & 0\\ G(L)^+ & F(L)^+ \end{bmatrix} \begin{bmatrix} \eta_t\\ v_t \end{bmatrix},$$
(29)

where  $U(L)^+ \equiv (1-L) U(L)$ ,  $G(L)^+ \equiv (1-L) G(L)$  and  $F(L)^+ \equiv (1-L) F(L)$ . Impulse responses can then be finally computed as  $I + \sum_{j=1}^k U_j^+$  for  $f_t$ , and

as 
$$I + \sum_{j=1}^{k} G_{j}^{+}$$
 and  $I + \sum_{j=1}^{k} F_{j}^{+}$  for  $x_{t} - \Lambda_{\mu}\mu_{t}, k = 1, 2, ...$ 

**Identification of structural shocks** The identification of the structural shocks in the FI-HF-VAR model can be implemented in two steps. Firstly, denoting by  $\xi_t$  the vector of the R structural common factor shocks, the relation between reduced and structural form common shocks can be written as  $\xi_t = H\eta_t$ , where H is square and invertible. Therefore, the identification of the structural common factor shocks amounts to the estimation of the elements of the H matrix. It is assumed that  $E[\xi_t \xi'_t] = I_R$ , and hence  $H\Sigma_{\eta}H' = I_R$ . As the number of free parameters in  $\Sigma_{\eta}$  is R(R+1)/2, at most R(R+1)/2 parameters in  $H^{-1}$  can be uniquely identified through the  $\Sigma_{\eta} = H^{-1} H^{\prime - 1}$  system of nonlinear equations in the unknown parameters of  $H^{-1}$ . Additional R(R-1)/2 restrictions need then to be imposed for exact identification of  $H^{-1}$ , by constraining the contemporaneous or long-run responses to structural shocks; for instance, recursive (Choleski) or non recursive structures can be imposed on the VAR model for the common factors through exclusion or linear/non-liner restrictions, as well as sign restrictions, on the contemporaneous impact matrix  $H^{-1}$ .<sup>5</sup>

Secondly, by denoting  $\varrho_t$  the vector of N structural idiosyncratic disturbances, the relation between reduced form and structural form idiosyncratic shocks can be written as  $\varrho_t = \Theta v_t$ , where  $\Theta$  is square and invertible. Hence, the identification of the structural idiosyncratic shocks amounts to the estimation of the elements of the  $\Theta$  matrix. It is assumed that  $E[\varrho_t \varrho'_t] = I_N$ , and hence  $\Theta \Sigma_v \Theta' = I_N$ . Then, in addition to the N(N+1)/2 equations provided by  $\Sigma = \Theta^{-1} \Theta'^{-1}$ , N(N-1)/2 restrictions need to be imposed for exact identification of  $\Theta^{-1}$ , similarly to what required for the common structural shocks.

Note that preliminary to the estimation of the  $\Sigma_v$  matrix,  $\hat{v}_t$  should be obtained from the residuals of an OLS regression of  $\hat{\varepsilon}_t$  on  $\hat{\eta}_t$ ; the latter operation would grant orthogonality between common and idiosyncratic residuals.

The structural VMA representation can then be written as

$$\begin{bmatrix} f_t \\ x_t - \Lambda_\mu \mu_t \end{bmatrix} = \begin{bmatrix} U^*(L) & 0 \\ G^*(L) & F^*(L) \end{bmatrix} \begin{bmatrix} \xi_t \\ \varrho_t \end{bmatrix}$$
(30)

where  $U^*(L) = U(L)H^{-1}$ ,  $G^*(L) = G(L)H^{-1}$ ,  $F^*(L) = F(L)\Theta^{-1}$ , or

$$(1-L)\begin{bmatrix} f_t\\ x_t - \Lambda_{\mu}\mu_t \end{bmatrix} = \begin{bmatrix} U^*(L)^+ & 0\\ G^*(L)^+ & F^*(L)^+ \end{bmatrix} \begin{bmatrix} \eta_t\\ v_t \end{bmatrix}, \quad (31)$$

where  $U^{*}(L)^{+} \equiv U(L)^{+}H^{-1}$ ,  $G^{*}(L)^{+} = G(L)^{+}H^{-1}$ ,  $F^{*}(L)^{+} = F(L)^{+}\Theta^{-1}$ , according to persistence properties, and  $E\left[\rho_{i,t}\xi'_{j,t}\right] = 0$  any i, j.

## 3 Estimation

Estimation of the model can be implemented following a multi-step procedure, consisting of persistence analysis, QML estimation of the common factors and VAR parameters in (1), QML estimation of the conditional mean model in (2) and the reduced form model in (24), QML estimation of the conditional variance covariance matrix in (2).

#### 3.1 Step 1: persistence analysis

Each component  $x_{i,t}$ , i = 1, ..., N, of the vector time series  $x_t$  is firstly decomposed into its purely deterministic (trend/break process;  $b_{i,t}$ ) and purely stochastic (break-free,  $l_{i,t} = x_{i,t} - b_{i,t}$ ) parts.

<sup>&</sup>lt;sup>5</sup>See Kilian (2011) for a recent survey.

It is then assumed that data obey the model

$$x_{i,t} = b_{i,t} + l_{i,t} \quad t = 1, ..., T \quad i = 1, ..., N,$$
(32)

where  $b_{i,t}$  and  $l_{i,t}$  are orthogonal,  $b_{i,t} \equiv z_{b,i}(t)$ , and  $z_{b,i}(t)$  is a bounded function of the time index t, evolving according to discontinuous changes (step function) or showing smooth transitions across regimes.

Depending on the specification of  $z_{b,i}(t)$ , a joint estimate of the two components can be obtained following Beran and Feng (2001, 2002a), Baillie and Morana (2012), Beran and Weiershauser (2011), Gonzalez and Terasvirta (2008), Hamilton (1989), by setting up an augmented fractionally integrated ARIMA model

$$\phi(L) \left(1 - L\right)^{d_i} \left( (1 - L)^k x_{i,t} - b_{i,t} \right) = v_{it},$$
(33)

where  $k = \{0, 1\}$  is the integer differencing parameter,  $d_i$ ,  $-0.5 < d_i < 0.5$ , is the fractional differencing parameter,  $\phi(L)$  is a stationary polynomial in the lag operator and  $v_{it}$  is a white noise disturbance. Heteroskedastic innovations can also be considered, by specifying  $v_{it} \equiv \sigma_{it}e_t$ , with  $e_t \sim i.i.d. (0, 1)$ , and the conditional variance process  $\sigma_{it}^2$  according to a model of the GARCH family.

Consistent and asymptotically normal estimation by means of QML, also implemented through iterative algorithms, is discussed in Beran and Feng (2002a,b), Baillie and Morana (2012), Beran and Weiershauser (2011), Perron and Varsnekov (2012). Extensions of the Markov switching (Hamilton, 1989), logistic (Gonzalez and Terasvirta, 2008) and random level shift models to the long memory case have also been contributed by Bordignon and Raggi (2010), Martens et al. (2003) and Grassi and de Magistris (2011), respectively.

Alternatively, the Bai and Perron (1989) two-step procedure can be followed: firstly, structural break tests are carried out and break points estimated; then, dummy variables are constructed according to their dating and the break process is estimated by running an OLS regression of the actual series  $x_{i,t}$  on the latter dummies, as in (3); this yields  $\hat{b}_{i,t}$  computed as the fitted process and the stochastic part as the estimated residual, i.e.,  $\hat{l}_{i,t} = x_{i,t} - \hat{b}_{i,t}$ .<sup>6</sup>

As neglected structural breaks may lead to processes which appear to show persistence of the long memory or unit root type (Perron, 1989; Granger and Hyung, 2004; Diebold and Inoue, 2001), as well as spurious breaks may

<sup>&</sup>lt;sup>6</sup>The orthogonality of  $\hat{b}_{i,t}$  and  $\hat{l}_{i,t}$  holds by construction when the break process is estimated by means of OLS, using break point dates as provided by testing. Orthogonality can however also be imposed when jointly estimating the deterministic and stochastic components by means of augmented ARFIMA models.

be detected in the data when persistence in the error component is neglected (Nunes et al., 1995; Bai, 1997; Kuan and Hsu, 1998), testing procedures robust to persistence properties are clearly desirable. In this respect, the Bai and Perron (1998) RSS-based testing framework allows consistent detection of multiple breaks at unknown dates for I(0) processes, as well as under long range dependence (Lavielle and Moulines, 2000)<sup>7</sup>; moreover, under long range dependence, the validity of an estimated break process (obtained, for instance, by means of the Bai-Perron tests) may also be assessed by testing the null hypothesis of long memory in the estimated break-free series  $(\hat{l}_{i,t})$ , as antipersistence is expected from the removal of a spurious break process (Granger and Hyung, 2004; Morana, 2014). Structural break tests valid for both I(0) and I(1) series have also been recently contributed by Kejiriwal and Perron (2010), Harvey et al. (2010), Bai and Carrion-i-Silvestre (2009) and Oka and Perron (2011).

#### 3.2 Step 2: Estimation of the conditional mean model

QML estimation of the reduced form model in (24) is achieved by first estimating the latent factors and VAR parameters in (1); then, by estimating the conditional mean process in (2); finally, by substituting (2) into (1) in order to obtain a restricted estimate of the polynomial matrix  $\Pi^*(L)$ .

#### 3.2.1 Estimation of the common factors and VAR parameters

Estimation of the common factors is performed by QML, writing the (misspecified) approximating model as

$$x_t - \Lambda_{\mu}\mu_t - \Lambda_f f_t = v_t$$

$$v_t \sim i.i.d.N.(0, \sigma^2 I_N)$$

$$f_t \sim i.i.d.N.(0, I_R),$$
(34)

with log-likelihood function given by

$$\ell\left(\cdot\right) = -\frac{NT}{2}\ln 2\pi - \frac{T}{2}\ln\left|\sigma^{2}I_{N}\right| - \frac{1}{2}\sum_{t=1}^{T}\frac{\left(x_{t} - \Lambda_{\mu}\mu_{t} - \Lambda_{f}f_{t}\right)'\left(x_{t} - \Lambda_{\mu}\mu_{t} - \Lambda_{f}f_{t}\right)}{\sigma^{2}}$$
(35)

<sup>&</sup>lt;sup>7</sup>Lavielle and Moulines (2000) have proved the strong consistency of the RSS estimator of the break fraction, independently of the rate of decay of the autocovariance function of the error process, when the number of break points is known; a modified Bayes-Schwarz criterion is then proposed for the selection of the number of break points.

QML estimation of the latent factors and their loadings then requires the minimization of the objective function

$$\sum_{t=1}^{T} \left( x_t - \Lambda_{\mu} \mu_t - \Lambda_f f_t \right)' \left( x_t - \Lambda_{\mu} \mu_t - \Lambda_f f_t \right), \tag{36}$$

which can be rewritten as

$$\frac{1}{NT} \sum_{t=1}^{T} \left( b_t - \Lambda_{\mu} \mu_t \right)' \left( b_t - \Lambda_{\mu} \mu_t \right) + \frac{1}{NT} \sum_{t=1}^{T} \left( l_t - \Lambda_f f_t \right)' \left( l_t - \Lambda_f f_t \right), \quad (37)$$

where  $x_t = l_t + b_t$ , as  $l_t$  and  $b_t$  are orthogonal vectors, as well as  $\mu_t$  and  $f_t$ .

The solution to the minimization problem, subject to the constraints

$$N^{-1}\Lambda'_{\mu}\Lambda_{\mu} = I_M \tag{38}$$

$$N^{-1}\Lambda'_f\Lambda_f = I_R, (39)$$

is given by firstly minimizing with respect to  $\mu_t$  and  $f_t$ , given  $\Lambda_{\mu}$  and  $\Lambda_f$ , yielding

$$\hat{\mu}_t \left( \Lambda_\mu \left( \Lambda'_\mu \Lambda_\mu \right)^{-1} \right) = \left( \Lambda'_\mu \Lambda_\mu \right)^{-1} \Lambda'_\mu b_t \hat{f}_t \left( \Lambda_f \left( \Lambda'_f \Lambda_f \right)^{-1} \right) = \left( \Lambda'_f \Lambda_f \right)^{-1} \Lambda'_f l_t,$$

and then concentrating the objective function to obtain

$$\frac{1}{T}\sum_{t=1}^{T}b_{t}'\left(I_{N}-\Lambda_{\mu}\left(\Lambda_{\mu}'\Lambda_{\mu}\right)^{-1}\Lambda_{\mu}\right)b_{t}+\frac{1}{T}\sum_{t=1}^{T}l_{t}'\left(I_{N}-\Lambda_{f}\left(\Lambda_{f}'\Lambda_{f}\right)^{-1}\Lambda_{f}\right)l_{t},$$
(40)

which can be mimized with respect to  $\Lambda_{\mu}$  and  $\Lambda_{f}$ . This is equivalent to maximizing

$$tr\left\{\left(\Lambda'_{\mu}\Lambda_{\mu}\right)^{-1/2'}\Lambda'_{\mu}\left(\frac{1}{T}\sum_{t=1}^{T}b_{t}b'_{t}\right)\Lambda_{\mu}\left(\Lambda'_{\mu}\Lambda_{\mu}\right)^{-1/2}\right\}+\tag{41}$$

$$tr\left\{\left(\Lambda_{f}^{\prime}\Lambda_{f}\right)^{-1/2\prime}\Lambda_{f}^{\prime}\left(\frac{1}{T}\sum_{t=1}^{T}l_{t}l_{t}^{\prime}\right)\Lambda_{f}\left(\Lambda_{f}^{\prime}\Lambda_{f}\right)^{-1/2}\right\},\tag{42}$$

which in turn is equivalent to maximizing

$$\Lambda_{\mu}\hat{\Sigma}_{b}\Lambda_{\mu} \tag{43}$$

(44)

subject to

$$N^{-1}\Lambda'_{\mu}\Lambda_{\mu} = I_M$$

$$\Lambda_f \hat{\Sigma}_l \Lambda_f \tag{44}$$

and

subject to

$$N^{-1}\Lambda'_f\Lambda_f = I_R.$$

The solution is then found by setting:

•  $\hat{\Lambda}_{\mu}$  equal to the scaled eigenvectors of  $\hat{\Sigma}_{b}$ , i.e., the sample variance covariance matrix of the break processes  $b_t$ , associated with its M largest eigenvalues; this yields  $\hat{\mu}_t = N^{-1} \hat{\Lambda}'_{\mu} b_t$ , i.e., the scaled first M principal components of  $b_t$ ;

•  $\hat{\Lambda}_{f}$  equal to the scaled eigenvectors of  $\hat{\Sigma}_{l}$ , i.e., the sample variance covariance matrix of the break-free processes  $l_t$ , corresponding to its R largest eigenvalues; this yields  $\hat{f}_t = N^{-1} \hat{\Lambda}'_f l_t$ , i.e., the scaled first R principal components of  $l_t$ .

Note that PCA uniquely estimates the space spanned by the unobserved factors; hence,  $\Lambda_f$  and  $f_t$  ( $\Lambda_{\mu}$  and  $\mu_t$ ) are not separately identified, as the common factors  $f_t(\mu_t)$  and factor loading matrix  $\Lambda_f(\Lambda_{\mu})$  are uniquely estimated up to a suitable invertible rotation matrix  $H_f(H_{\mu})$ , i.e., PCA delivers estimates of  $f_{*,t} \equiv H_f f_t$   $(\mu_{*,t} \equiv H_\mu \mu_t)$  and  $\Lambda_{f_*} \equiv \Lambda_f H_f^{-1}$   $(\Lambda_{\mu_*} \equiv \Lambda_\mu H_\mu^{-1}),$ and therefore a unique estimate of the common components  $\Lambda_f f_t \equiv \Lambda_{f_*} f_{*,t}$  $(\Lambda_{\mu}\mu_t \equiv \Lambda_{\mu_*}\mu_{*,t})$  only, which is however all what is required for the computation of the gap vector.

As shown by Bai and Ng (2013), exact identification of the common factors can also be implemented, by appropriately constraining the factor loading matrix while performing PCA or after estimation. In particular, three identification structures are discussed, involving a block diagonal factor loading matrix, yield by a statistical restriction imposed in estimation, and two rotation strategies, yielding a lower triangular factor loading matrix in the former case and a two-block partitioned factor loading matrix in the latter case, with identity matrix in the upper block and an unrestricted structure in the lower block.

Moreover, the number of common factors (R, M) is unknown and needs to be determined; several criteria are available in the literature, ranging from heuristic or statistical eigenvalue-based approaches (Jackson, 1993; Kapetanios, 2010; Cragg and Donald, 1997; Gill and Lewbel, 1992, Robin and Smith, 2000; see also Peres-Neto et al., 2005), to the variance test of Connor and Korajczyk (1993), and the more recent information criteria (Stock and Watson, 1998; Forni et al., 2000; Bai and Ng, 2002) and "primitive" shock (Bai and Ng, 2007; Stock and Watson, 2005) based procedures.

Finally, in order to enforce orthogonality between the estimated common break processes  $(\hat{\mu}_{*,t})$  and stochastic factors  $(\hat{f}_{*,t})$ , the above procedure may be modified by computing the stochastic component  $\hat{l}_t$  as the residuals from the OLS regression of  $x_t$  on  $\hat{\mu}_{*,t}$ ; then PCA is implemented on  $\hat{l}_t$  to yield  $\hat{f}_{*,t}$ .

Estimation of the VAR parameters. Conditional on the estimated (rotated) latent factors, the polynomial matrix C(L) and  $\Lambda_{f_*} \equiv \Lambda_f H_f^{-1}$  and  $\Lambda_{\mu_*} \equiv \Lambda_\mu H_\mu^{-1}$  (rotated) factor loading matrices are obtained by means of OLS estimation of the equation system in (1). This can be obtained by first (OLS) regressing the actual series  $x_t$  on the estimated common break processes  $(\hat{\mu}_{*,t})$ and stochastic factors  $(\hat{f}_{*,t})$  to obtain  $\hat{\Lambda}_{\mu_*}$  and  $\hat{\Lambda}_{f_*}$ ; alternatively,  $\Lambda_{\mu_*}$  and  $\Lambda_{f_*}$  can be estimated as yield by PCA, i.e., from the scaled eigenvectors of the matrices  $\hat{\Sigma}_b$  and  $\hat{\Sigma}_l$ , respectively; then, the gap vector is computed as  $x_t - \hat{\Lambda}_{\mu_*}\hat{\mu}_{*,t} - \hat{\Lambda}_{f_*}\hat{f}_{*,t}$ , as  $\hat{\Lambda}_f \hat{f}_t \equiv \hat{\Lambda}_{f_*}\hat{f}_{*,t}$  and  $\hat{\Lambda}_{\mu}\hat{\mu}_t \equiv \hat{\Lambda}_{\mu_*}\hat{\mu}_{*,t}$ , and  $\hat{C}(L)$  is obtained by means of OLS estimation of the VAR model in (1).

#### 3.2.2 Iterative estimation of the common factors and VAR parameters

The above estimation strategy may be embedded within an iterative procedure, yielding a (relatively more efficient) estimate of the latent factors and the VAR parameters in the equation system in (1).

The objective function to be minimized is then written as

$$S\left(\Lambda_{\mu}, \mu_{t}, \Lambda_{f}, f_{t}, C(L)\right) = \frac{1}{NT} \sum_{t=1}^{T} v_{t}^{\prime} v_{t}$$

$$(45)$$

where  $v_t = (I_N - C(L)L) (x_t - \Lambda_\mu \mu_t - \Lambda_f f_t)$ .

• Initialization. The iterative estimation procedure requires an initial estimate of the common deterministic  $(\mu_t)$  and stochastic  $(f_t)$  factors and the C(L) polynomial matrix, i.e., an initial estimate of the equation system in (1). The latter can be obtained as described in Section 3.2.1.

• Updating. An updated estimate of the equation system in (1) is obtained as follows.

•• First, a new estimate of the M (rotated) common deterministic factors, and their factor loading matrix, is obtained by the application of PCA to the (new) stochastic factor-free series  $x_t - \hat{\Lambda}_{f_*} \hat{f}_{*,t} - \hat{C}(L) \left( x_{t-1} - \hat{\Lambda}_{f_*} \hat{f}_{*,t-1} - \hat{\Lambda}_{\mu_*} \hat{\mu}_{*,t-1} \right)$ yielding  $\hat{\Lambda}_{\mu_*}^{(new)}$  and  $\hat{\mu}_{*,t}^{(new).8}$ 

•• Next, conditional on the new common break processes and their factor loading matrix, the new estimate of the common long memory factors is obtained from the application of PCA to the (new) break-free processes  $\hat{l}_{t}^{(new)} = x_{t} - \hat{\Lambda}_{\mu_{*}}^{(new)} \hat{\mu}_{*,t}^{(new)9}, \text{ yielding } \hat{\Lambda}_{f_{*}}^{(new)} \text{ and } \hat{f}_{*,t}^{(new)10}$ •• Finally, conditional on the new estimated common break processes

and long memory factors, the new estimate of the gap vector  $x_t - \hat{\Lambda}_{\mu_*}^{(new)} \hat{\mu}_{*,t}^{(new)} - \hat{\Lambda}_{\mu_*}^{(new)} \hat{\mu}_{*,t}^{(new)}$  $\hat{\Lambda}_{f_*}^{(new)} \hat{f}_{*,t}^{(new)}$  is obtained, and the new estimate  $\hat{C}(L)^{(new)}$  can be computed by means of OLS estimation of the VAR model in (1).

•• The above procedure is iterated until convergence, yielding the final estimates  $\hat{\Lambda}_{\mu_*}^{(fin)}$ ,  $\hat{\mu}_{*,t}^{(fin)}$ ,  $\hat{\Lambda}_{f_*}^{(fin)}$ ,  $\hat{f}_{*,t}^{(fin)}$ , and  $\hat{C}(L)^{(fin)}$ .<sup>11</sup>

#### 3.2.3Restricted estimation of the reduced form model

Once the final estimate of the equation system in (1) is available, the reduced VAR form in (24) is estimated as follows:

i) for the case of fractional integration (long memory)  $(0 < d_i < 1)$ , the fractional differencing parameter is (consistently) estimated first, for each component of the (rotated) common factors vector  $\hat{f}_{*,t}^{(fin)}$ , yielding the estimates  $\hat{d}_i$ , i = 1, ..., R, collected in  $\hat{D}(L)$  matrix.

Considering then the generic element  $\hat{f}_{*i,t}^{(fin)}$ ,  $\sqrt{T}$  consistent and asymptotically normal estimation of the *i*th fractional differencing parameter can be obtained, for instance, by means of QML estimation of the fractionally integrated ARIMA model in (33), i.e.,

$$\phi(L) (1-L)^{d_i} (1-L)^k \hat{f}_{*i,t}^{(fin)} = \eta_{it};$$
(46)

<sup>&</sup>lt;sup>8</sup>Alternatively,  $\hat{\Lambda}_{\mu_*}^{(new)}$  can be obtained by regressing  $x_t$  on  $\hat{\mu}_{*,t}^{(new)}$  (and the initial estimate  $\hat{f}_{*,t}$ ), using OLS.

<sup>&</sup>lt;sup>9</sup>Alternatively, the new break-free process can be computed as  $x_t - \hat{\Lambda}_{\mu_*}\hat{\mu}_{*,t}$  –

 $<sup>\</sup>hat{C}(L)\left(x_{t-1} - \hat{\Lambda}_{f_*}\hat{f}_{*,t-1} - \hat{\Lambda}_{\mu_*}\hat{\mu}_{*,t-1}\right).$ <sup>10</sup>Alternatively,  $\hat{\Lambda}_{f_*}^{(new)}$  can be obtained by regressing  $x_t$  on  $\hat{f}_{*,t}^{(new)}$  and the updated estimate  $\hat{\mu}_{*,t}^{(new)}$ , using OLS. This would also yield a new estimate  $\hat{\Lambda}_{\mu_*}^{(new)}$  to be used in the computation of the updated gap vector.

<sup>&</sup>lt;sup>11</sup>For instance, the procedure can be stopped when  $c_{j+1} = \frac{S(\hat{\theta}^{(j+1)}) - S(\hat{\theta}^{(j)})}{S(\hat{\theta}^{(j+1)}) + S(\hat{\theta}^{(j)})} < -10^{-4},$ where the objective function is written as in (45).

alternatively, consistent and asymptotically normal estimation can be obtained by means of the log-periodogram regression or the Whittle-likelihood function.<sup>12</sup>

Then, conditionally to the estimated fractionally differencing parameter,  $\hat{P}(L)$  is obtained by means of OLS estimation of the VAR(u) model for the fractionally differenced common factors  $(\hat{D}(L)\hat{f}_{*,t}^{(fin)})$  in (2); hence,  $I - \hat{\Pi}(L) = \hat{P}(L)\hat{D}^*(L)$ , where  $\hat{D}^*(L)$  is the  $R \times R$  diagonal polynomial matrix in the lag operator containing the  $p^*$ th order  $(p^* > u)$  truncated binomial expansion of the elements in  $\hat{D}(L)$ . Then,  $\hat{\Pi}_f^*(L) = \hat{\Pi}(L)L^{-1}$  and  $\hat{\Pi}^*(L) = [\hat{\Lambda}_f^{(fin)}\hat{\Pi}(L)L^{-1} - \hat{C}(L)^{(fin)}\Lambda_f^{(fin)}]$ .

Alternatively, rather than by means of the two-step Box-Jenkins type of approach detailed above, system estimation can be performed by setting up a multivariate version of the model in (46)

$$\Phi(L)D(L)(1-L)^{k}\hat{f}_{*i,t}^{(fin)} = \eta_{t}, \qquad (47)$$

where  $\Phi(L)$  is a finite order stationary polynomial matrix in the lag operator, yielding  $\sqrt{T}$  consistent and asymptotically normal estimation performed by means of Conditional-Sum-of-Squares (Robinson, 2006), exact Maximum Likelihood (Sowell, 1992) or Indirect (Martin and Wilkins, 1999) estimation.<sup>13</sup> OLS estimation of a VAR approximation for the VARFIMA model in (47) has also been recently proposed by Baillie and Kapetanios (2013), which would even avoid the estimation of the fractional differencing parameter for the common stochastic factors. Moreover,

*ii*) for the case of no integration (short memory)  $(d_i = 0)$ ,  $\hat{P}(L)$  is obtained by means of OLS estimation of the VAR(u) model for the (rotated) common stochastic factors  $(\hat{f}_{*,t}^{(fin)})$  in (2); then  $\hat{\Pi}(L) = \hat{P}_1L + \hat{P}_2L^2 + ... + \hat{P}_uL^u$ ;

*iii*) for the I(1) case  $(d_i = 1)$ ,  $\hat{\Gamma}(L)$  is obtained by means of OLS estimation of the VAR(u+1) model in levels for the (rotated) common stochastic factors  $(\hat{f}_{*,t}^{(fin)})$ , implied by (2), taking into account (26) and (27); then,  $\hat{\Pi}(L) = \hat{\Gamma}_1 L + \hat{\Gamma}_2 L^2 + \ldots + \hat{\Gamma}_{u+1} L^{u+1}$ .

Consistent with Bai and Ng (2006, 2008), in all of the above cases VAR estimation can be performed as the estimated common factors were actually observed.

Following the thick modelling strategy of Granger and Jeon (2004), median estimates of the parameters of interest, impulse responses and forecast

 $<sup>^{12}</sup>$ See Nielsen and Frederiksen (2005) and Chan and Palma (2006) for a survey of alternative estimators of the fractional differencing parameter.

<sup>&</sup>lt;sup>13</sup>Depending on the parametric structure, system estimation may however become unfeasible when the number of factors is too large.

error variance decomposition, as well as their confidence intervals, can be computed through simulation.

### 3.3 Step 3: Estimation of the conditional variancecovariance matrix

The estimation of the conditional variance-covariance matrix for the factors in (2) can be carried out using a procedure similar to the O-GARCH model of Alexander (2002):

i) firstly, conditional variance estimation is carried out factor by factor, using the estimated factor residuals  $\hat{\eta}_t$ , yielding  $\hat{h}_{i,t}$ , i = 1, 2, ..., R; QML estimation can be performed in a variety of settings, ranging from standard GARCH(p,q) (Bollerslev, 1986) and FIGARCH(p,b,z) (Baillie et al., 1996) models to their "adaptive" generalizations (Engle and Rangel, 2008; Baillie and Morana, 2009; Amado and Terasvirta, 2008; Hamilton and Susmel, 1994), in order to allow for different sources of persistence in variance;

*ii*) secondly, consistent with the assumption of conditional and unconditional orthogonality of the factors, the conditional variance-covariance  $(H_{x,t})$  and correlation  $(R_{x,t})$  matrices for the actual series may be estimated as

$$\hat{H}_{x,t} = \hat{\Lambda}_f \hat{H}_t \hat{\Lambda}_f' + \hat{\Sigma}_v \tag{48}$$

$$\hat{R}_{x,t} = \hat{H}_{x,t}^{*-1/2} \hat{H}_{x,t} \hat{H}_{x,t}^{*-1/2}, \qquad (49)$$

where  $\hat{H}_t = diag \left\{ \hat{h}_{1,t}, \hat{h}_{2,t}, ..., \hat{h}_{R,t} \right\}$  and  $\hat{H}^*_{x,t} = diag \left\{ \hat{h}_{x_1,t}, \hat{h}_{x_2,t}, ..., \hat{h}_{x_N,t} \right\}$ .

Relaxing the assumption of conditional orthogonality of the factors is also feasible in the proposed framework, as the dynamic conditional covariances, i.e., the off-diagonal elements in  $H_t$ , can be obtained, after step *i*) above, by means of the second step in the estimation of the Dynamic Conditional Correlation model (DCC; Engle, 2002) or the Dynamic Equicorrelation model (DECO; Engle and Kelly, 2012).

#### **3.4** Asymptotic properties

The proposed iterative procedure for the system of equations in (1) bears the interpretation of QML estimation, using a Gaussian likelihood function, performed by means of the EM algorithm (Dempster et al., 1977). In the E-step, the unobserved factors are estimated, given the observed data and the current estimate of model parameters, by means of PCA; in the M-step the likelihood function is maximized (OLS estimation of the C(L) matrix is performed) under the assumption that the unobserved factors are known, conditioning on their *E*-step estimate. Convergence to the one-step QML estimate is ensured, as the value of the likelihood function is increased at each step (see Quah and Sargent, 1992; Watson and Engle, 1983). The latter implementation of the EM algorithm follows from considering the estimated factors by PCA as they were actually observed. In fact, the *E*-step would also require the computation of the conditional expectation of the estimated factors, which may be obtained by means of Kalman smoothing (Doz et al., 2011, 2012). As shown by Bai and Ng (2006, 2008), however, when the unobserved factors are estimated by means of PCA in the *E*-step, the generated regressors problem is not an issue for consistent estimation in the *M*-step, due to faster vanishing of the estimation error, provided  $\sqrt{T}/N \rightarrow 0$  for linear models, and  $T^{5/8}/N \rightarrow 0$  for (some classes of) non linear models, i.e., the factors estimated by means of PCA can be considered as they where actually observed, therefore not requiring a Kalman smoothing step.

Note also that the *Expectation* step of the *EM* algorithm relies on consistent estimation of the unobserved components. In this respect, under general conditions,  $min\left\{\sqrt{N}, \sqrt{T}\right\}$  consistency and asymptotic normality of PCA, at each point in time, for the unobserved common components  $\Lambda_f f_t$ , has been established by Bai (2003, 2004) for  $N, T \to \infty$  and the case of I(0) and I(1) unobserved components;<sup>14</sup> this implies the consistent estimation

<sup>&</sup>lt;sup>14</sup>In particular, under some general conditions, given any invertible matrix  $\Xi$ ,  $\sqrt{N}$  consistency and asymptotic normality of PCA for  $\Xi f_t$ , at each point in time, is established for  $N, T \to \infty$  and  $\sqrt{N}/T \to 0$  and the case of I(0) unobserved factors and idiosyncratic components, the latter also displaying limited heteroskedasticity in both their time-series and cross-sectional dimensions (Bai, 2003); for  $N, T \to \infty$  and  $N/T^3 \to 0$  and the case of I(1) (non cointegrated) unobserved factors and I(0) idiosyncratic components, similarly showing limited heteroskedasticity in both the time-series and cross-sectional dimensions (Bai, 2004). The latter result is actually obtained by applying PCA to the level of the series, rather than their first differences. Moreover, for both the I(0) and I(1) case,  $\sqrt{T}$  consistency and asymptotic normality of PCA for  $\Lambda_f \Xi^{-1}$  is established under the same conditions, as well as  $min \left\{ \sqrt{N}, \sqrt{T} \right\}$  consistency and asymptotic normality of PCA for the unobserved common components  $\Lambda_f f_t$ , at each point in time, for  $N, T \to \infty$ .

The conditions for consistency and asymptotic normality reported in Bai (2003, 2004) implicitly cover also the case in which PCA is implemented using the *estimated* break  $(\hat{b}_t)$ and break-free  $(\hat{l}_t \equiv x_t - \hat{b}_t)$  components, rather than the observed  $x_t$  series; in fact, by assuming  $\hat{b}_t = b_t + e_{b,t}$  and  $\hat{l}_t = l_t + e_{l,t}$ , then  $\hat{b}_t = \Lambda_\mu \mu_t + e_{b,t}$  and  $\hat{l}_t = \Lambda_f f_t + e_{l,t}$ , which are static factor structures as assumed in Bai (2003, 2004). It appears that assumption E in Bai (2003, pag.143), i.e., weak dependence and limited cross-sectional correlation, holding for both noise (estimation error) components  $e_{b,t}$  and  $e_{l,t}$ , augmented with the assumption of their contemporaneous orthogonality, i.e.,  $E[e_{b,t}e'_{l,t}] = 0$ , is then sufficient for the validity of PCA also when implemented on noisy data. In this respect PCA acts as noise suppressor: intuitively, PCs associated with the smallest eigenvalues are noise, which should be neglected when estimating the common factors. PCA estimation of the

of the gap vector  $x_t - \Lambda_\mu \mu_t - \Lambda_f f_t$ , at the same  $\min \left\{ \sqrt{N}, \sqrt{T} \right\}$  rate, for  $N, T \to \infty$ , as well. Based on the results for I(0) and I(1) processes, the same properties can be conjectured also for the intermediate cases of long memory and (linear/nonlinear) trend stationarity; supporting Monte Carlo evidence is actually provided by Morana (2007) and in this study.<sup>15</sup>

Moreover, likewise in the Maximization step of the EM algorithm,  $\sqrt{T}$  consistent and asymptotically normal estimation of the polynomial matrix C(L) is yield by OLS estimation of the VAR model for the I(0) gap vector  $x_t - \Lambda_\mu \mu_t - \Lambda_f f_t^{16}$ , which, according to the results in Bai and Ng (2006, 2008), can be taken as it were actually observed in the implementation of the iterative estimation procedure.

Similarly,  $\sqrt{T}$  consistent and asymptotically normal estimation of the block of equations in (2) is obtained by means of OLS estimation of the conditional mean process first, holding the estimated latent factors as they were observed, still relying on the results in Bai and Ng (2006, 2008) and on a consistent estimate of the fractional differencing parameter if needed, and then performing QML estimation of the conditional variance-covariance matrix.

### 4 Monte Carlo analysis

Consider the following data generation process (DGP) for the  $N \times 1$  vector process  $x_t$ 

$$x_{t} - \Lambda_{\mu}\mu_{t} - \Lambda_{f}f_{t} = C(x_{t-1} - \Lambda_{\mu}\mu_{t-1} - \Lambda_{f}f_{t-1}) + v_{t}$$
(50)  
$$v_{t} \sim i.i.d.(0, \sigma^{2}I_{N}),$$

where C is a  $N \times N$  matrix of coefficients,  $\Lambda_{\mu}$  and  $\Lambda_{f}$  are  $N \times 1$  vectors of loadings, and  $\mu_{t}$  and  $f_{t}$  are the common deterministic and long memory factors, respectively, at time period t, with

$$(1 - \phi L)(1 - L)^d f_t = \eta_t.$$
(51)

Then, for the conditionally heteroskedastic case it is assumed

signal component can actually be shown optimal in terms of minimum mean square error (see, for instance, Castells et al., 2007).

<sup>&</sup>lt;sup>15</sup>The use of PCA for the estimation of common deterministic trends has previously been advocated by Hatanaka and Yamada (2004). See also Langsang and Barrios for applications to nonstationary data.

<sup>&</sup>lt;sup>16</sup>Note that the gap vector  $x_t - \Lambda_{\mu}\mu_t - \Lambda_f f_t$  is I(0), independently of the integration order of the actual series  $x_t$ .

$$\eta_t = \sqrt{h_t}\psi_t \qquad \psi_t \sim iid(0,1)$$
$$[1 - \alpha L - \beta L](1 - L)^b \left(\eta_t^2 - \sigma_\eta^2\right) = [1 - \beta L] \left(\eta_t^2 - h_t\right), \tag{52}$$

while

$$\eta_t \sim i.i.d.(0,1) \tag{53}$$

for the conditionally homoskedastic case.

Different values for the autoregressive idiosyncratic parameter  $\rho$ , common across the N cross-sectional units ( $C = \rho I_N$ ), have been considered, i.e.,  $\rho =$  $\{0, 0.2, 0.4, 0.6, 0.8\}$ , as well as for the fractionally differencing parameter d = $\{0, 0.2, 0.4, 0.6, 0.8, 1\}$  and the common factor autoregressive parameter  $\phi$ , setting  $\phi = \{0.2, 0.4, 0.6, 0.8\}$  for the non integrated case and  $\phi = \{0, d/2\}$  for the fractionally integrated and integrated cases;  $\phi > \rho$  is always assumed in the experiment. For the conditional variance equation it is assumed  $\alpha = 0.05$ and  $\beta = 0.90$  for the short memory case, and  $\alpha = 0.05$ ,  $\beta = 0.30$  and b = 0.45for the long memory case. The inverse signal to noise ratio ( $s/n^{-1}$ ) is given by  $\sigma^2/\sigma_{\eta}^2$ , taking values  $s/n^{-1} = \{4, 2, 1, 0.5, 0.25\}$ . Finally,  $\Lambda_{\mu}$  and  $\Lambda_f$  are set equal to unitary vectors.

Moreover, in addition to the structural stability case, i.e.,  $\mu_t = \mu = 0$ , two designs with breaks have been considered for the component  $\mu_t$ , i.e.,

*i*) the single step change in the intercept at the midpoint of the sample case, i.e.,

$$\mu_t = \begin{cases} 0 & t = 1, ..., T/2 \\ 4 & t = T/2 + 1, ..., T \end{cases};$$

*ii*) the two step changes equally spaced throughout the sample case, with the intercept increasing at one third of the way through the sample and then decreasing at a point two thirds of the length of the sample, i.e.,

$$\mu_t = \begin{cases} 0 & t = 1, ..., T/3 \\ 4 & t = T/3 + 1, ..., 2T/3 \\ 2 & t = 2T/3 + 1, ..., T \end{cases}$$

The sample size investigated is T = 100, 500, and the number of cross-sectional units is N = 30. For the no breaks case also other cross-sectional sample sizes have been employed, i.e., N = 5, 10, 15, 50.

The number of replications has been set to 2,000 for each case.

The performance of the proposed multi-step procedure has then been assessed with reference to the estimation of the unobserved common stochastic and deterministic factors, and the  $\phi$  and  $\rho$  autoregressive parameters. Concerning the estimation of the common factors, the Theil's inequality coefficient (*IC*) and the correlation coefficient (*Corr*) have been employed in the evaluation, i.e.,

$$IC = \sqrt{\frac{1}{T} \sum_{t=1}^{T} (z_t - \hat{z}_t)^2} / (\sqrt{\frac{1}{T} \sum_{t=1}^{T} z_t^2} + \sqrt{\frac{1}{T} \sum_{t=1}^{T} \hat{z}_t^2}),$$
  

$$Corr = Cov(z_t, \hat{z}_t) / \sqrt{Var(z_t)Var(\hat{z}_t)},$$

where  $z_t = \mu_t$ ,  $f_t$  is the population unobserved component and  $\hat{z}_t$  its estimate. The above statistics have been computed for each Monte Carlo replication and then averaged.

In the Monte Carlo analysis, the location of the break points and the value of the fractional differencing parameter are taken as known, in order to focus on the assessment on the estimation procedure contributed by the paper; the break process is then estimated by means of the OLS regression approach of Bai and Perron (1998). The Monte Carlo evidence provided is then comprehensive concerning the no-breaks I(0) and I(1) cases, as well as for the no-break I(d) case, concerning the estimation of the common stochastic factor. A relative assessment of the various methodologies which can be employed for the decomposition into break and break-free components is however of interest and left for further research.

#### 4.1 Results

The results for the non integration case are reported in Figures 1-2 (and 5, columns 1 and 3), while Figures 3-4 (and 5, columns 2 and 4) refer to the fractionally integrated and integrated cases (the *integrated* case, independent of the type of integration, thereafter). In all cases results refer to the estimated parameters for the first equation in the model. Since the results are virtually unaffected by the presence of conditional heteroskedasticity, for reasons of space, only the heteroskedastic case is discussed. Moreover, only the results for the  $\phi = d/2$  case are reported for the integrated case, as similar results have been obtained for the  $\phi = 0$  case.<sup>17</sup>

#### 4.1.1 The structural stability case

As shown in Figure 5 (top plots 1-4), for a cross-sectional sample size N = 30 units, a negligible downward bias for the  $\rho$  parameter (on average across (inverse) signal to noise ratio values) can be noted (-0.02 and -0.03, for the non integrated and integrated case, respectively, and T = 100 (top plots 1-2);

<sup>&</sup>lt;sup>17</sup>See the Appendix for detailed results.

-0.01 and -0.006, respectively, and T = 500 (top plots 3-4)), decreasing as the serial correlation spread,  $\phi - \rho$  or  $d - \rho$ , or the sample size T increase.

Differently, as shown in Figures 1 and 3 (top plots 1 and 3), the downward bias in  $\phi$  is increasing with the degree of persistence of the common factor d, the (inverse) signal to noise ratio  $s/n^{-1}$ , and the serial correlation spread,  $\phi - \rho$  or  $d - \rho$ , yet decreasing with the sample size T.

For the non integrated case (Figure 1, plots 1 and 3), there are only few cases ( $\phi - \rho = 0.4, 0.6, 0.8$ ) when a 10%, or larger, bias in  $\phi$  is found, occurring when the series are particularly noisy ( $s/n^{-1} = 4$ ); for the stationary long memory case a 10% bias, or smaller, is found for  $s/n^{-1} \ge 2$ , while for the non stationary long memory case for  $s/n^{-1} \ge 1$  and a (relatively) large sample (T = 500) (Figure 3, plots 1 and 3). Increasing the cross-sectional dimension N yields improvements (see the next section).

Also, as shown in Figures 2 and 4 (top plots 1-4), very satisfactory is the estimation of the unobserved common stochastic factor, as the *IC* statistic is always below 0.2 (0.14 (0.10), on average, for T = 100 (T = 500) for the non integrated case (Figure 2, top plots 2 and 4); 0.06 (0.03), on average, for T = 100 (T = 500) for the integrated case (Figure 4, top plots 2 and 4)). Moreover, the correlation coefficient between the actual and estimated common factors is always very high, 0.98 and 0.99, on average, respectively, for both sample sizes (Figures 2 and 4, top plots 1 and 3).

Results for smaller and larger cross-sectional samples In Figures 1-2 and 3-4 (center plots, i.e., rows 2 and 3) the bias for the  $\phi$  parameter and the correlation coefficient between the actual and estimated common factors are also plotted for different cross-sectional dimensions, i.e., N = 5, 10, 15, 50, for the non integrated and integrated cases, respectively; statistics for the  $\rho$  parameter are not reported, as the latter is always unbiasedly estimated, independently of the cross-sectional dimension.

As is shown in the plots, the performance of the estimator crucially depends on T, N, and  $s/n^{-1}$ .

For the non integrated case (Figure 1), when the (inverse) signal to noise ratio is low, i.e.,  $s/n^{-1} \leq 0.5$ , the downward bias is already mitigated by using a cross-sectional sample size as small as N = 5, for T = 100; as Nincreases, similar results are obtained for higher  $s/n^{-1}$ , i.e., N = 10, 15 and  $s/n^{-1} \leq 1$ , or N = 50 and  $s/n^{-1} \leq 4$  (center plots, column 1-2). For a larger sample size, i.e., T = 500 (center plots, column 3-4), similar conclusions hold, albeit for the N = 5 the (inverse) signal to noise ratio can be higher, i.e.,  $s/n^{-1} \leq 1$ ; similarly for N = 10, 15 with  $s/n^{-1} \leq 2$ .

For the integrated case (Figure 3) conditions are slightly more restrictive;

in particular, for the stationary long memory case, when the (inverse) signal to noise ratio is low, i.e.,  $s/n^{-1} \leq 0.5$ , the downward bias is already mitigated by setting N = 5 and T = 100; similar results are obtained for higher  $s/n^{-1}$ and N, i.e., N = 10, 15 and  $s/n^{-1} \leq 1, 2$ , or N = 50 and  $s/n^{-1} \leq 4$ (center plots, column 1-2). Similar conclusions can be drawn for T = 500(center plots, column 3-4), albeit, holding N constant, accurate estimation is obtained also for higher  $s/n^{-1}$ . Similarly also for the non stationary case (long memory or I(1)); yet, holding T constant, either larger N, or lower  $s/n^{-1}$ , would be required for accurate estimation.

Coherently, the correlation coefficients between the actual and estimated common factors (Figures 2 and 4, center plots), point to satisfactory estimation (a correlation coefficient higher than 0.9) also in the case of a small temporal sample size, provided the (inverse) signal to noise ratio is not too high, and/or the cross-sectional dimension is not too low  $(s/n^{-1} \leq 1 \text{ and } N = 5; s/n^{-1} \leq 2 \text{ and } N = 10; s/n^{-1} \leq 4 \text{ and } N = 15).$ 

#### 4.1.2 The structural change case

While concerning the estimation of the  $\rho$  parameter no sizable differences can be found for the designs with structural change, relatively to the case of structural stability<sup>18</sup>, the complexity of the break process may on the other hand affect estimation accuracy for the  $\phi$  parameter, worsening as the number of break points increases, particularly when the temporal sample size is small (T = 100).

Yet, for the no integration case (Figure 1, bottom plots) already for T = 500 the performance is very satisfactory for both designs, independently of the (inverse) signal to noise ratio  $s/n^{-1}$  (bottom plots, columns 3 and 4); differently, for T = 100 the performance is satisfactory (at most a 10% bias) only when the series are not too noisy  $(s/n^{-1} \leq 1)$  (bottom plots, columns 1 and 2). Also, similar to the structural stability case, the (downward) bias in the  $\phi$  parameter is increasing with the degree of persistence of the common factor d, the (inverse) signal to noise ratio  $s/n^{-1}$ , and  $\phi - \rho$  or  $d - \rho$ , yet decreasing with the sample size T.

Coherent with the above results, satisfactory estimation of the unobserved common stochastic factor (Figure 2, bottom plots) and break process can also be noted (Figure 5, bottom plots, columns 1 and 3); for the common stochastic factor, the IC statistic (not reported) is in fact always below 0.2

<sup>&</sup>lt;sup>18</sup>The average bias is -0.04 and -0.01, independent of the break process design and integration properties, when T = 100 and T = 500, respectively. Moreover, similar to the structural stability case the bias is decreasing as  $\phi - \rho$ ,  $d - \rho$ , or the sample size T increase, independent of the (inverse) signal to noise ratio.

for T = 500 (0.11 and 0.13, on average, for the single break point and twobreak points case, respectively) and below 0.3 for T = 100 (0.17 and 0.20, on average; column 1), while the actual and estimated common stochastic factors are strongly correlated: for T = 100 (T = 500), on average, the correlation coefficient is 0.96 (0.98) for the single break point case and 0.93 (0.97) for the two-break points case (column 3).

Very accurate is also the estimation of the common break process: the IC statistic is never larger than 0.15 for T = 100 and 0.075 for T = 500 (Figure 5, bottom plots, columns 1 and 3), while the correlation coefficient is virtually 1 for the single break case and never below 0.96 for T = 100 and 0.99 for T = 500 for the two-break points case (not reported). Given the assumption of known break points, the performance in terms of correlation coefficient is not surprising; yet, the very small Theil's index is indicative of the ability of the modeling approach to recover the changing level of the unobserved common break process.

Concerning the integrated case, some differences relatively to the non integrated case can be noted; as shown in Figure 5 (bottom plots, columns 2 and 4), albeit the overall recovery of the common break process is always very satisfactory across the various designs, independently of the sample size (the IC statistic is never larger than 0.14; bottom plots), performance slightly worsens as the complexity of the break process and persistence intensity (d) increase: the average correlation coefficient between the estimated and actual break processes (center plots) falls from 1 when d = 0.2 (single break point case) to 0.93 when d = 1 (two-break points case).

Moreover, concerning the estimation of the common stochastic factor (Figure 4, center and bottom plots, columns 1-4), for the covariance stationary case (d < 0.5) results are very close to the non integrated case, i.e., an *IC* statistic (not reported) always below 0.2 for T = 500 (0.12 and 0.14, on average, for the single break point and two-break points case, respectively) and below 0.3 for T = 100 (0.21 and 0.24, on average, respectively); the correlation coefficient is also very high: 0.94 and 0.91, on average, T = 100 (columns 1 and 2); 0.97 and 0.96, on average, T = 500 (columns 3 and 4).

Differently, for the non stationary case performance is worse, showing average IC statistics (not reported) of 0.32 (0.32) and 0.42 (0.44), respectively, for the single break point (center plots) and two-break points (bottom plots) case and T = 100 (T = 500); the average correlation coefficient is 0.79 (0.78) and 0.68 (0.66), respectively. Coherently, a worsening in the estimation of the common factor autoregressive parameter  $\phi$ , for the d = 0.8 and d = 1case, can be noted (Figure 3, center and bottom plots), while comparable results to the short memory case can be found for d < 0.5. The latter findings are however not surprising, as the stronger the degree of persistence of the stochastic component (and of the series, therefore) and the less accurate the disentangling of the common break and break-free parts can be expected; overall, the Monte Carlo results point to accurate decompositions also for the case of moderate nonstationary long memory, albeit deterioration in performance becomes noticeable.

## 5 Conclusions

In the paper a general strategy for large-scale modeling of macroeconomic and financial data, set within the factor vector autoregressive model (F-VAR) framework, is introduced. The proposed approach shows minimal pretesting requirements, performing well independently of integration properties of the data and sources of persistence, i.e., deterministic or stochastic, accounting for common features of different kinds, i.e., common integrated (of the fractional or integer type) or non integrated stochastic factors, also heteroskedastic, and common deterministic break processes. Consistent and asymptotically normal estimation is performed by means of QML, implemented through an iterative multi-step algorithm. Monte Carlo results strongly support the proposed approach. Empirical implementations can be found in Morana (2013, 2014), Cassola and Morana (2012) and Bagliano and Morana (2014), showing the approach being easy to implement and effective also in the case of very large systems of dynamic equations.

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Figure 1: In the figure, Monte Carlo bias and RMSE statistics for the autoregressive parameter ( $\phi$ ) are plotted for the case of no breaks (top and center plots) and one (break 1) and two (break 2) breaks (bottom plots), and a conditionally heteroskedastic common I(0) factor. Results are reported for various values of the persistence spread  $\phi$ - $\rho$  (0.2, 0.4, 0.6, 0.8) against various values of the (inverse) signal to noise ratio (s/n)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size **T** is 100 and 500 observations, the number of cross-sectional units **N** is 30, and the number of replications for each case is 2,000. For the no breaks case, Monte Carlo bias statistics are also reported for other sample sizes N (5, 10, 15, 50) (center plots).



Figure 2: In the figure, Monte Carlo Carlo Theil's index (IC) and correlation coefficient (Corr) statistics, concerning the estimation of the conditionally heteroskedastic common I(0) factor, are plotted for the case of no breaks (top and center plots) and one (break 1) and two (break 2) breaks (bottom plots). Results are reported for various values of the persistence spread **\Phi-\rho** (0.2, 0.4, 0.6, 0.8) against various values of the (inverse) signal to noise ratio (**s/n**)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size **T** is 100 and 500 observations, the number of cross-sectional units **N** is 30, and the number of replications for each case is 2,000. For the no breaks case, Monte Carlo correlation coefficient statistics are also reported for other sample sizes **N** (5, 10, 15, 50) (center plots).



Figure 3: In the figure, Monte Carlo bias statistics for the autoregressive parameter ( $\phi$ ) are plotted for the case of no breaks (top and center plots) and one (break 1) and two (break 2) breaks (center and bottom plots), and a conditionally heteroskedastic common I(d) factor ( $0 < d \le 1$ ). Results are reported for various values of the persistence spread **d-p** (0.2, 0.4, 0.6, 0.8, 1) against various values of the (inverse) signal to noise ratio (**s/n**)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size **T** is 100 and 500 observations, the number of cross-sectional units **N** is 30, and the number of replications for each case is 2,000. For the no breaks case, Monte Carlo bias statistics are also reported for other sample sizes N (5, 10, 15, 50) (center plots).



Figure 4: In the figure Monte Carlo Carlo correlation coefficient (Corr) statistics, concerning the estimation of the conditionally heteroskedastic common I(d) factor ( $0 < d \le 1$ ), are plotted for the case of no breaks (top and center plots) and one (break 1) and two (break 2) breaks (bottom plots). Results are reported for various values of the persistence spread **d**-**p** (0.2, 0.4, 0.6, 0.8, 1) against various values of the (inverse) signal to noise ratio (s/n)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size **T** is 100 and 500 observations, the number of cross-sectional units **N** is 30, and the number of replications for each case is 2,000. For the no breaks case, Monte Carlo correlation coefficient statistics are also reported for other sample sizes N (5, 10, 15, 50) (center plots).



Figure 5: In the figure, average Monte Carlo statistics (across values for the inverse signal to noise ratio) for the bias in the autoregressive idiosyncratic parameter ( $\rho$ ) (top plots) and Theil's index (IC) statistic for the common break process (bottom plots) are plotted for the non integrated (I(0)) and integrated (I(d),  $0 < d \le 1$ ) cases. Results are reported for various values of the persistence spreads  $\phi$ - $\rho$  (0.2, 0.4, 0.6, 0.8) and d- $\rho$  (0.2, 0.4, 0.6, 0.8, 1). The sample size **T** is 100 and 500 observations, the number of cross-sectional units **N** is 30, and the number of replications for each case is 2,000.

#### **Appendix: Monte Carlo results.**

autoregressive common factor parameter ø		
hias		
Ulus		
$T = 100  \phi = 0.2 \qquad \phi = 0.4 \qquad \phi = 0.6 \qquad \phi$	= 0.8	
$(s/n)^{-1}$ $\rho = 0$ $\rho = 0$ $\rho = 0.2$ $\rho = 0$ $\rho = 0.2$ $\rho = 0.4$ $\rho = 0$ $\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4 -0.037 -0.063 -0.035 -0.078 -0.060 -0.037 -0.075 -0.064	-0.054	-0.038
2 -0.028 -0.044 -0.030 -0.055 -0.047 -0.038 -0.055 -0.050	-0.047	-0.039
1 -0.021 -0.033 -0.027 -0.044 -0.040 -0.036 -0.045 -0.042	-0.041	-0.039
0.5 -0.019 -0.027 -0.025 -0.037 -0.035 -0.034 -0.039 -0.039	-0.037	-0.037
<b>0.25</b> -0.017 -0.025 -0.023 -0.033 -0.032 -0.032 -0.036 -0.036	-0.036	-0.036
root mean square error		
$T = 100$ $\phi = 0.2$ $\phi = 0.4$ $\phi = 0.6$ $d$	= 0.8	
$(s/n)^{-1}$ $\rho = 0$ $\rho = 0$ $\rho = 0.2$ $\rho = 0$ $\rho = 0.2$ $\rho = 0.4$ $\rho = 0$ $\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
<i>4</i> 0.116 0.133 0.106 0.144 0.123 0.099 0.132 0.118	0.104	0.083
<b>2</b> 0.110 0.115 0.105 0.119 0.110 0.102 0.107 0.101	0.097	0.088
<i>1</i> 0.108 0.107 0.103 0.108 0.103 0.100 0.096 0.093	0.091	0.088
<b>0.5</b> 0.107 0.103 0.102 0.102 0.100 0.099 0.090 0.089	0.088	0.087
<b>0.25</b> 0.107 0.102 0.101 0.099 0.098 0.098 0.087 0.086	0.086	0.086
autoregressive parameter p		
bias		
$T = 100$ $\phi = 0.2$ $\phi = 0.4$ $\phi = 0.6$ $d$	= 0.8	
$(s/n)^{-1}$ $\rho = 0$ $\rho = 0$ $\rho = 0.2$ $\rho = 0$ $\rho = 0.2$ $\rho = 0.4$ $\rho = 0$ $\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4 -0.010 -0.011 -0.021 -0.017 -0.024 -0.034 -0.018 -0.026	-0.033	-0.040
2 -0.012 -0.014 -0.020 -0.014 -0.022 -0.034 -0.019 -0.025	-0.036	-0.046
1 -0.010 -0.016 -0.025 -0.016 -0.026 -0.034 -0.021 -0.028	-0.040	-0.042
<b>0.5</b> -0.011 -0.013 -0.022 -0.017 -0.024 -0.035 -0.016 -0.026	-0.036	-0.044
<b>0.25</b> -0.012 -0.019 -0.022 -0.018 -0.023 -0.031 -0.018 -0.021	-0.035	-0.047
root mean sauare error		
$T = 100  \phi = 0.2 \qquad \phi = 0.4 \qquad \phi = 0.6 \qquad d$	= 0.8	
$\begin{bmatrix} s/n \end{bmatrix}^{-1} & o = 0 & o = 0 & o = 0 & 2 & o = 0 & o = 0 & 2 & o = 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0$	$\rho = 0.4$	$\rho = 0.6$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 103	0 102
2 0.103 0.100 0.103 0.098 0.107 0.106 0.103 0.105	0.108	0.102
2 0100 0100 0100 0100 0100	0.100	0.104
1 0.101 0.105 0.107 0.104 0.107 0.107 0.105 0.104	0.107	
1         0.101         0.105         0.107         0.104         0.107         0.107         0.105         0.104           0.5         0.102         0.101         0.103         0.104         0.104         0.107         0.102         0.104	0.107	0.105
1         0.101         0.105         0.107         0.104         0.107         0.107         0.105         0.104           0.5         0.102         0.101         0.103         0.104         0.104         0.107         0.107         0.102         0.104           0.5         0.102         0.101         0.103         0.104         0.104         0.107         0.102         0.104           0.25         0.100         0.102         0.104         0.102         0.104         0.106         0.100         0.104	0.107 0.107 0.106	0.105
1         0.101         0.105         0.107         0.104         0.107         0.107         0.105         0.104           0.5         0.102         0.101         0.103         0.104         0.104         0.107         0.107         0.102         0.104           0.25         0.100         0.102         0.104         0.102         0.104         0.106         0.100         0.104           autorgressive common factor parameter \$\phi\$	0.107 0.107 0.106	0.105 0.110
I         0.101         0.105         0.107         0.104         0.107         0.107         0.105         0.104           0.5         0.102         0.101         0.103         0.104         0.104         0.107         0.102         0.104           0.25         0.100         0.102         0.104         0.102         0.104         0.106         0.100         0.104           autoregressive common factor parameter φ           bias	0.107 0.107 0.106	0.104
1 $0.101$ $0.105$ $0.107$ $0.104$ $0.107$ $0.107$ $0.105$ $0.104$ 0.5 $0.102$ $0.101$ $0.103$ $0.104$ $0.104$ $0.107$ $0.102$ $0.104$ 0.25 $0.100$ $0.102$ $0.104$ $0.102$ $0.104$ $0.106$ $0.100$ $0.104$ autoregressive common factor parameter $\phi$ bias         T = 500 $\phi = 0.4$ $\phi = 0.6$ $\phi$	0.107 0.107 0.106	0.105 0.110
1       0.101       0.105       0.107       0.104       0.107       0.107       0.105       0.104         0.5       0.102       0.101       0.103       0.104       0.104       0.107       0.102       0.104         0.25       0.100       0.102       0.104       0.102       0.104       0.106       0.100       0.104         autoregressive common factor parameter $\phi$ bias         T = 500 $\phi = 0.2$ $\phi = 0.4$ $\phi = 0.6$ $\phi$ <td>= 0.8</td> <td>0.104 0.105 0.110</td>	= 0.8	0.104 0.105 0.110
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$= 0.8$ $\rho = 0.4$ -0.028	$\rho = 0.6$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $\rho = 0.4$ -0.028 -0.018	$\rho = 0.6$ -0.020 -0.014
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $= 0.8$ $= 0.028$ $= 0.013$	$\rho = 0.6$ -0.020 -0.014 -0.011
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $\rho = 0.4$ -0.028 -0.018 -0.013	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $\rho = 0.4$ -0.028 -0.013 -0.010 -0.008	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $= 0.8$ $= 0.000$ $= 0.4$ $= 0.018$ $= -0.018$ $= -0.013$ $= -0.010$ $= -0.008$	$\rho = 0.6$ -0.020 -0.014 -0.001 -0.008
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	= 0.8 $= 0.8$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$	$\rho = 0.6$ -0.020 -0.014 -0.009 -0.008
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $= 0.8$ $= 0.0107$ $= 0.4$ $= 0.010$ $= 0.013$ $= 0.013$ $= 0.010$ $= 0.8$ $= 0.8$ $= 0.4$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $= 0.8$ $= 0.4$ $= 0.8$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.8$ $= 0.8$ $= 0.4$ $= 0.51$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.041
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 -0.013 -0.010 -0.016 = 0.8 -0.018 -0.013 -0.010 -0.008 = 0.8 $\rho = 0.4$ -0.028 -0.010 -0.008 = 0.8 $\rho = 0.4$ 0.051 0.040	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.041 0.036
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $= 0.8$ $= 0.4$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.001$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 -0.008 -0.008 -0.008 -0.008 -0.036 -0.036 -0.034 -0.036 -0.034 -0.03
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $= 0.8$ $= 0.8$ $= 0.028$ $= 0.010$ $= 0.010$ $= 0.0010$ $= 0.0010$ $= 0.8$ $= 0.8$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.51$ $= 0.40$ $= 0.40$ $= 0.35$ $= 0.33$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.041 0.036 0.034 0.033
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 0.107 \\ 0.107 \\ 0.106 \\ \end{array}$ $\begin{array}{c} = 0.8 \\ \rho = 0.4 \\ -0.028 \\ -0.013 \\ -0.013 \\ -0.010 \\ -0.008 \\ \end{array}$ $\begin{array}{c} = 0.8 \\ \rho = 0.4 \\ 0.051 \\ 0.040 \\ 0.035 \\ 0.033 \\ 0.032 \end{array}$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.041 0.036 0.034 0.033 0.032
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$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} 0.107 \\ 0.107 \\ 0.106 \end{array}$ $= 0.8 \\ \rho = 0.4 \\ -0.028 \\ -0.013 \\ -0.010 \\ -0.008 \\ \hline \rho = 0.4 \\ 0.051 \\ 0.040 \\ 0.035 \\ 0.033 \\ 0.032 \\ \end{array}$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.041 0.036 0.034 0.033 0.032
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $= 0.8$ $= 0.8$ $= 0.028$ $= 0.010$ $= 0.4$ $= 0.013$ $= 0.013$ $= 0.010$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0000$ $= 0.0000$ $= 0.0000$ $= 0.0000$ $= 0.0000$ $= 0.0000$ $= 0.0000$ $= 0.0000$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.034 0.033 0.032 $\rho = 0.6$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.8 $= 0.8$ $= 0.8$ $= 0.010$ $= 0.4$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.8$ $= 0.4$ $= 0.0013$ $= 0.8$ $= 0.8$ $= 0.8$ $= 0.8$ $= 0.8$ $= 0.4$ $= 0.0013$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.034 0.033 0.032 $\rho = 0.6$ -0.011
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.107 0.107 0.107 0.106 $= 0.8$ $= 0.8$ 0.013 -0.018 -0.013 -0.010 -0.008 $= 0.8$ $p = 0.4$ 0.051 0.040 0.035 0.033 0.032 $= 0.8$ $p = 0.4$ -0.007 -0.006	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.041 0.036 0.034 0.033 0.032 $\rho = 0.6$ -0.011 -0.011
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$= 0.107$ 0.107 0.107 0.107 0.106 $= 0.8$ $\rho = 0.4$ -0.028 -0.018 -0.013 -0.010 -0.008 $= 0.8$ $\rho = 0.4$ 0.051 0.040 0.035 0.033 0.032 $= 0.8$ $\rho = 0.4$ -0.007 -0.006 -0.008	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.034 0.033 0.032 $\rho = 0.6$ -0.011 -0.011 -0.001 -0.011 -0.001
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	= 0.107 0.107 0.107 0.106 $= 0.8$ $= 0.4$ -0.028 -0.013 -0.010 -0.008 $= 0.8$ $p = 0.4$ 0.051 0.040 0.035 0.033 0.032 0.032 $= 0.8$ $p = 0.4$ -0.007 -0.008 -0.007	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.034 0.033 0.032 $\rho = 0.6$ -0.011 -0.001 -0.009 -0.009
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} 0.107 \\ 0.107 \\ 0.107 \\ 0.106 \\ \end{array}$ $\begin{array}{c} = 0.8 \\ \rho = 0.4 \\ -0.028 \\ -0.018 \\ -0.013 \\ -0.010 \\ -0.008 \\ \end{array}$ $\begin{array}{c} = 0.8 \\ \rho = 0.4 \\ 0.051 \\ 0.040 \\ 0.035 \\ 0.032 \\ \end{array}$ $\begin{array}{c} = 0.8 \\ \rho = 0.4 \\ -0.007 \\ -0.006 \\ -0.007 \\ -0.007 \\ -0.007 \\ -0.007 \\ -0.007 \\ -0.007 \\ \end{array}$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.034 0.033 0.032 $\rho = 0.6$ -0.011 -0.011 -0.011 -0.009 -0.009 -0.010
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	= 0.8 $= 0.8$ $= 0.8$ $= 0.010$ $= 0.4$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0013$ $= 0.0007$ $= 0.0007$ $= 0.0007$ $= 0.0007$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.034 0.033 0.032 $\rho = 0.6$ -0.011 -0.011 -0.011 -0.009 -0.009 -0.009 -0.009 -0.009 -0.010
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	= 0.107 0.107 0.107 0.106 $= 0.8$ $= 0.8$ 0.013 -0.018 -0.013 -0.010 -0.008 $= 0.8$ $p = 0.4$ 0.051 0.040 0.035 0.033 0.032 $= 0.8$ $p = 0.4$ -0.007 -0.006 -0.008 -0.007 -0.007 -0.007 = 0.8	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.034 0.033 0.032 0.032 $\rho = 0.6$ -0.011 -0.011 -0.009 -0.009 -0.009 -0.009 -0.009 -0.010
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	= 0.107 0.107 0.107 0.106 $= 0.8$ $= 0.4$ -0.028 -0.018 -0.013 -0.010 -0.008 $= 0.8$ $p = 0.4$ 0.051 0.040 0.035 0.033 0.032 $= 0.8$ $p = 0.4$ -0.007 -0.006 -0.008 -0.007 -0.007 $= 0.8$ $p = 0.4$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.034 0.033 0.032 $\rho = 0.6$ -0.011 -0.011 -0.009 -0.009 -0.009 -0.009 -0.009 -0.010 $\rho = 0.6$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$= 0.107$ 0.107 0.107 0.106 $= 0.8$ $\rho = 0.4$ -0.028 -0.018 -0.013 -0.010 -0.008 $= 0.8$ $\rho = 0.4$ 0.051 0.040 0.035 0.033 0.032 0.04 0.007 0.007 0.007 0.007 0.007 0.007 0.002 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.042 0.04 0.04	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.033 0.032 $\rho = 0.6$ -0.011 -0.011 -0.011 -0.011 -0.011 -0.011 -0.009 -0.009 -0.009 -0.010 -0.010 -0.010 -0.010 -0.010 -0.039
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	= 0.8 $= 0.8$ $= 0.8$ $= 0.000$ $= 0.4$ $= 0.000$ $= 0.4$ $= 0.000$ $= 0.4$ $= 0.000$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.007$ $= 0.007$ $= 0.007$ $= 0.8$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$ $= 0.4$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.031 0.032 $\rho = 0.6$ -0.011 -0.011 -0.011 -0.011 -0.011 -0.011 -0.009 -0.009 -0.009 -0.009 -0.010 $\rho = 0.6$ 0.039 0.040
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	= 0.8 $\rho = 0.4$ -0.028 -0.018 -0.013 -0.010 -0.008 = 0.8 $\rho = 0.4$ 0.010 -0.008 = 0.8 $\rho = 0.4$ 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.035 0.032 $\rho = 0.4$ -0.007 -0.006 -0.007 -0.0042 -0.042 -0.043 -0.043	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.041 0.036 0.034 0.033 0.032 $\rho = 0.6$ -0.011 -0.011 -0.011 -0.009 -0.009 -0.009 -0.009 -0.010 -0.010 -0.010 -0.010 -0.038
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} 0.107 \\ 0.107 \\ 0.107 \\ 0.106 \\ \end{array}$ $\begin{array}{c} = 0.8 \\ \rho = 0.4 \\ -0.028 \\ -0.013 \\ -0.013 \\ -0.010 \\ -0.008 \\ \end{array}$ $\begin{array}{c} = 0.8 \\ \rho = 0.4 \\ 0.051 \\ 0.040 \\ 0.035 \\ 0.033 \\ 0.032 \\ \end{array}$ $\begin{array}{c} = 0.8 \\ \rho = 0.4 \\ -0.007 \\ -0.006 \\ -0.007 \\ -0.007 \\ -0.007 \\ \end{array}$ $\begin{array}{c} = 0.8 \\ \rho = 0.4 \\ 0.042 \\ 0.042 \\ 0.042 \\ 0.042 \\ 0.042 \\ 0.042 \\ 0.042 \\ 0.042 \end{array}$	$\rho = 0.6$ -0.020 -0.014 -0.011 -0.009 -0.008 $\rho = 0.6$ 0.034 0.033 0.032 $\rho = 0.6$ -0.011 -0.011 -0.009 -0.009 -0.009 -0.009 -0.009 -0.009 -0.010 $\rho = 0.6$ 0.034 0.032

Table 1: No structural break, heteroskedastic case, N=30: bias and RMSE of parameters

The Table reports Monte Carlo bias and RMSE statistics concerning the estimation of the common factor ( $\phi$ ) and idiosyncratic ( $\rho$ ) autoregressive parameters. Results are reported for various values of the common factor autoregressive parameter  $\phi$  (0, 2, 0.4, 0.6, 0.8), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0.2, 0.4, 0.6), assuming  $\phi > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 30, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved autoregressive factor and no breaks.

Table 2: 1	No structur	al break,	heteroskea	lastic cas	e, N=30: M	onte Carlo	) Theil an	d correlati	ion statistic	s	
					N=30						
				autoregre	essive comn	non factor					
					Theil index	c					
T = 100	$\phi = 0.2$	φ=	= 0.4		$\phi = 0.6$			φ =	= 0.8		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	
4	0.187	0.183	0.185	0.174	0.176	0.185	0.175	0.177	0.182	0.195	
2	0.140	0.140	0.142	0.139	0.141	0.146	0.153	0.154	0.158	0.165	
1	0.108	0.111	0.112	0.116	0.117	0.121	0.140	0.141	0.143	0.147	
0.5	0.086	0.092	0.093	0.102	0.102	0.105	0.132	0.132	0.133	0.136	
0.25	0.072	0.081	0.081	0.093	0.093	0.095	0.127	0.127	0.128	0.130	
				corre	lation coef	ficient					
T = 100	$\phi = 0.2$	φ=	= 0.4		$\phi = 0.6$	$\phi = 0.8$					
$(s/n)^{-1}$	$\rho = 0$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	
4	0.938	0.944	0.943	0.956	0.955	0.949	0.973	0.972	0.968	0.959	
2	0.968	0.972	0.971	0.978	0.977	0.974	0.986	0.986	0.984	0.979	
1	0.984	0.986	0.985	0.989	0.988	0.987	0.993	0.993	0.992	0.990	
0.5	0.992	0.993	0.993	0.994	0.994	0.993	0.997	0.996	0.996	0.995	
0.25	0.996	0.996	0.996	0.997	0.997	0.997	0.998	0.998	0.998	0.997	
					Theil index	c					
T = 500	$\phi = 0.2$	φ=	= 0.4		$\phi = 0.6$		$\phi = 0.8$				
(s/n) <sup>-1</sup>	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	
4	0.176	0.167	0.170	0.150	0.152	0.162	0.126	0.128	0.135	0.150	
2	0.127	0.121	0.124	0.111	0.113	0.119	0.099	0.100	0.105	0.115	
1	0.093	0.089	0.091	0.084	0.085	0.090	0.081	0.082	0.085	0.092	
0.5	0.068	0.067	0.068	0.066	0.067	0.070	0.070	0.071	0.073	0.077	
0.25	0.052	0.052	0.053	0.054	0.054	0.056	0.063	0.064	0.065	0.067	
				corre	lation coef	ficient					
T = 500	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	= 0.8		
$(s/n)^{-1}$	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	
4	0.941	0.948	0.946	0.959	0.958	0.952	0.976	0.975	0.972	0.964	
2	0.969	0.973	0.972	0.979	0.978	0.975	0.988	0.987	0.986	0.981	
1	0.984	0.986	0.986	0.989	0.989	0.988	0.994	0.994	0.993	0.991	
0.5	0.992	0.993	0.993	0.995	0.994	0.994	0.997	0.997	0.996	0.995	
0.25	0.996	0.997	0.996	0.997	0.997	0.997	0.999	0.998	0.998	0.998	

The Table reports Monte Carlo *Theil index and correlation coefficient* statistics concerning the estimation of the unobserved common factor component. Results are reported for various values of the common factor autoregressive parameter  $\phi$  (0.2, 0.4, 0.6, 0.8), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0.2, 0.4, 0.6), assuming  $\phi > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 30, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved autoregressive factor and no breaks.

	igie break	ooini, neie	roskeuusu	c case, N-	30: bias an	a KMSE 0	j purumet	ers		
					N=30					
			autore	gressive c	ommon fac	ctor param	eter ø			
					Bias					
T = 100	$\phi = 0.2$	φ =	0.4		$\phi = 0.6$			φ =	= 0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	-0.050	-0.078	-0.051	-0.099	-0.078	-0.057	-0.101	-0.091	-0.079	-0.062
2	-0.038	-0.058	-0.045	-0.076	-0.066	-0.057	-0.080	-0.076	-0.071	-0.064
1	-0.031	-0.047	-0.042	-0.062	-0.060	-0.055	-0.070	-0.068	-0.066	-0.064
0.5	-0.028	-0.042	-0.039	-0.056	-0.054	-0.053	-0.064	-0.064	-0.063	-0.062
0.5	-0.020	0.020	0.039	-0.050	-0.054	-0.053	-0.004	-0.004	-0.005	-0.002
0.23	-0.027	-0.039	-0.038	-0.055	-0.032	-0.052	-0.002	-0.001	-0.001	-0.001
				root m	ean square	error?				
T = 100	$\phi = 0.2$	φ =	0.4		$\phi = 0.6$			φ =	= 0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.125	0.151	0.123	0.170	0.143	0.119	0.166	0.151	0.135	0.111
2	0.118	0.130	0.118	0.142	0.130	0.120	0.138	0.132	0.125	0.116
1	0.113	0.120	0.117	0.127	0.124	0.120	0.125	0.122	0.119	0.117
0.5	0.111	0.116	0.115	0.121	0.119	0.118	0.118	0.117	0.116	0.115
0.25	0.111	0.115	0.114	0.117	0.117	0.116	0.114	0.115	0.114	0.114
				autoregi	ressive para	ımeter p				
					bias					
T = 100	$\phi = 0.2$	<i>d</i> =	0.4		$\phi = 0.6$			<i>ф</i> =	= 0.8	
$(s/n)^{-1}$	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	n = 0.2	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
(3/1)	0.021	0.023	0.036	0.027	0.035	0.048	0.031	0.040	0.050	0.064
7	-0.021	-0.025	-0.030	-0.027	-0.035	-0.040	-0.031	-0.040	-0.050	-0.004
2	0.021	0.029	0.033	0.020	-0.038	-0.049	0.034	0.041	-0.051	-0.002
1	-0.025	-0.025	-0.038	-0.028	-0.031	-0.048	-0.022	-0.033	-0.031	-0.003
0.5	-0.025	-0.025	-0.034	-0.028	-0.038	-0.049	-0.034	-0.035	-0.049	-0.063
0.25	-0.020	-0.026	-0.035	-0.027	-0.033	-0.051	-0.027	-0.035	-0.048	-0.063
				root m	ean square	error ?				
T = 100	$\phi = 0.2$	φ =	÷ 0.4		$\phi = 0.6$			φ =	= 0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.104	0.108	0.112	0.106	0.110	0.117	0.110	0.115	0.121	0.126
2	0.106	0.108	0.109	0.106	0.113	0.117	0.110	0.114	0.120	0.126
1	0.103	0.106	0.112	0.107	0.107	0.118	0.106	0.113	0.120	0.129
0.5	0.105	0.108	0.111	0.106	0.111	0.118	0.111	0.111	0.116	0.126
0.25	0.106	0.105	0.112	0.108	0.111	0.121	0.108	0.111	0.118	0.126
0.20	0.100	0.100	autona	anassina a	ommon far	**** <b>n</b> auau	0.100	0.111	0.110	0.120
			autore	gressive c	hias	tor param	eler <i>φ</i>			
<b>T</b> 500	1 0 2	,	autore	gressive c	bias	tor purum	eier φ	1	0.0	
T = 500	$\phi = 0.2$	φ=	0.4	gressive c	$bias$ $\phi = 0.6$	tor purum		φ =	= 0.8	
T = 500 (s/n) <sup>-1</sup>	$\phi = 0.2$ $\rho = 0$	$\phi = \rho = 0$	$0.4$ $\rho = 0.2$	$\rho = 0$	$bias$ $\phi = 0.6$ $\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\phi = \rho = 0.2$	= 0.8 $\rho = 0.4$	$\rho = 0.6$
$T = 500$ $(s/n)^{-1}$ $4$	$\phi = 0.2$ $\rho = 0$ -0.028	$\phi = \rho = \theta$ -0.048	$\rho = 0.2$ -0.027	$\rho = 0$ -0.057	$bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ 0.027 \\ \phi = 0.2 \\ 0.037 \\ \phi $	$\rho = 0.4$ -0.026	$\rho = 0$ -0.049	$\phi = \rho = 0.2$ -0.040	= $0.8$ $\rho = 0.4$ -0.033	<i>ρ</i> = 0.6 -0.024
T = 500 (s/n) <sup>-1</sup> 4 2	$\phi = 0.2$ $\rho = 0$ -0.028 -0.018	$\phi = \phi$ -0.048 -0.029	$0.4$ $\rho = 0.2$ -0.027 -0.019	p = 0 -0.057 -0.034	$bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ -0.027 \\ 0.027 \\$	p = 0.4 -0.026 -0.019	$\rho = 0$ -0.049 -0.030	$\phi = 0.2$ -0.040 -0.026	$= 0.8$ $\rho = 0.4$ -0.033 -0.022	<i>ρ</i> = 0.6 -0.024 -0.018
T = 500 (s/n) <sup>-1</sup> 4 2 1	φ = 0.2 ρ = 0 -0.028 -0.018 -0.012	φ = ρ = 0 -0.048 -0.029 -0.018	= 0.4 $p = 0.2$ $-0.027$ $-0.019$ $-0.013$	p = 0 -0.057 -0.034 -0.022	$bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ -0.027 \\ -0.019 \\ \hline$	p = 0.4 -0.026 -0.019 -0.015	p = 0 -0.049 -0.030 -0.021	φ = ρ = 0.2 -0.040 -0.026 -0.018	$= 0.8$ $\rho = 0.4$ -0.033 -0.022 -0.017	<i>ρ</i> = 0.6 -0.024 -0.018 -0.015
T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5	$\phi = 0.2$ $\rho = 0$ -0.028 -0.018 -0.012 -0.009	φ = ρ = θ -0.048 -0.029 -0.018 -0.013	$ \begin{array}{c} \textbf{a} \textbf{a} \textbf{b} \textbf{c} \textbf{c} \textbf{c} \textbf{c} \textbf{c} \textbf{c} \textbf{c} c$	p = 0 -0.057 -0.034 -0.022 -0.016	$bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ -0.027 \\ -0.019 \\ -0.014 \\ end{tabular}$	$\rho = 0.4$ -0.026 -0.019 -0.015 -0.012	$\rho = 0$ -0.049 -0.030 -0.021 -0.016	φ = ρ = 0.2 -0.040 -0.026 -0.018 -0.015	<b>ο.8</b> <b>ρ = 0.4</b> -0.033 -0.022 -0.017 -0.014	<i>ρ</i> = 0.6 -0.024 -0.018 -0.015 -0.013
T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25	φ = 0.2 ρ = 0 -0.028 -0.018 -0.012 -0.009 -0.007	φ = ρ = θ -0.048 -0.029 -0.018 -0.013 -0.010	θ.4           ρ = 0.2           -0.027           -0.019           -0.013           -0.011           -0.009	$\rho = \theta$ -0.057 -0.034 -0.022 -0.016 -0.013	$bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ -0.027 \\ -0.019 \\ -0.014 \\ -0.012 \\ contract c$	p = 0.4 -0.026 -0.019 -0.015 -0.012 -0.011	$\rho = 0$ -0.049 -0.030 -0.021 -0.016 -0.013	φ = ρ = 0.2 -0.040 -0.026 -0.018 -0.015 -0.013	<b>ο.8</b> <b>ρ = 0.4</b> -0.033 -0.022 -0.017 -0.014 -0.013	<b>p</b> = <b>0.6</b> -0.024 -0.018 -0.015 -0.013 -0.012
	φ = 0.2 ρ = 0 -0.028 -0.018 -0.012 -0.009 -0.007	φ = ρ = θ -0.048 -0.029 -0.018 -0.013 -0.010	p = 0.2 -0.027 -0.019 -0.013 -0.011 -0.009	$\rho = 0$ -0.057 -0.034 -0.022 -0.016 -0.013 root m	$bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ -0.027 \\ -0.019 \\ -0.014 \\ -0.012 \\ ean square$	p = 0.4 -0.026 -0.019 -0.015 -0.012 -0.011 e error	p = 0 -0.049 -0.030 -0.021 -0.016 -0.013	φ = ρ = 0.2 -0.040 -0.026 -0.018 -0.015 -0.013	<b>ρ</b> = <b>0.8</b> <b>ρ</b> = <b>0.4</b> -0.033 -0.022 -0.017 -0.014 -0.013	<i>ρ</i> = 0.6 -0.024 -0.018 -0.015 -0.013 -0.012
$     \begin{array}{r}       T = 500 \\       (s/n)^{-1} \\       4 \\       2 \\       1 \\       0.5 \\       0.25 \\       \hline       T = 500     \end{array} $	$\phi = 0.2$ $\rho = 0$ -0.028 -0.018 -0.012 -0.009 -0.007 $\phi = 0.2$	$\phi = 0$ -0.048 -0.029 -0.018 -0.013 -0.010 $\phi =$	$\begin{array}{c} 0.4 \\ \hline \rho = 0.2 \\ -0.027 \\ -0.019 \\ -0.013 \\ -0.011 \\ -0.009 \end{array}$	p = 0 -0.057 -0.034 -0.022 -0.016 -0.013 root m	$bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ -0.027 \\ -0.019 \\ -0.014 \\ -0.012 \\ ean square \\ \phi = 0.6 \\ equare baseline baselin$	p = 0.4 -0.026 -0.019 -0.015 -0.012 -0.011 e error	p = 0 -0.049 -0.030 -0.021 -0.016 -0.013	$\phi = 0.2$ -0.040 -0.026 -0.018 -0.015 -0.013 $\phi = 0.013$	<ul> <li>= 0.8</li> <li>-0.033</li> <li>-0.022</li> <li>-0.017</li> <li>-0.014</li> <li>-0.013</li> <li>= 0.8</li> </ul>	<i>ρ</i> = 0.6 -0.024 -0.018 -0.015 -0.013 -0.012
T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25 $T = 500$ (s/n) <sup>-1</sup>		$\phi = \theta \\ -0.048 \\ -0.029 \\ -0.018 \\ -0.013 \\ -0.010 \\ \phi = \theta$	$\begin{array}{c} 0.4 \\ \rho = 0.2 \\ -0.027 \\ -0.019 \\ -0.013 \\ -0.011 \\ -0.009 \\ \hline 0.4 \\ \rho = 0.2 \end{array}$	$\rho = 0$ -0.057 -0.034 -0.022 -0.016 -0.013 root m $\rho = 0$	$\begin{array}{c} bias \\ \hline bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ -0.027 \\ -0.019 \\ -0.014 \\ -0.012 \\ \hline ean square \\ \phi = 0.6 \\ \rho = 0.2 \end{array}$	$\rho = 0.4$ -0.026 -0.019 -0.015 -0.012 -0.011 e error $\rho = 0.4$	$\rho = \theta$ -0.049 -0.030 -0.021 -0.016 -0.013 $\rho = \theta$	$\phi = 0.2$ -0.040 -0.026 -0.018 -0.015 -0.013 $\phi = 0.2$	$= 0.8$ $\rho = 0.4$ -0.033 -0.022 -0.017 -0.014 -0.013 $= 0.8$ $\rho = 0.4$	$\rho = 0.6$ -0.024 -0.018 -0.015 -0.013 -0.012 $\rho = 0.6$
T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25 $T = 500$ (s/n) <sup>-1</sup> 4	$\phi = 0.2$ $\rho = 0$ -0.028 -0.018 -0.012 -0.009 -0.007 $\phi = 0.2$ $\rho = 0$ 0.060	$\phi = 0$ -0.048 -0.029 -0.018 -0.013 -0.010 $\phi = 0$ 0.081	$\begin{array}{c} \textbf{0.4} \\ \hline \textbf{\rho} = \textbf{0.2} \\ \textbf{-0.027} \\ \textbf{-0.019} \\ \textbf{-0.013} \\ \textbf{-0.011} \\ \textbf{-0.009} \\ \hline \textbf{0.4} \\ \hline \textbf{\rho} = \textbf{0.2} \\ \textbf{0.059} \end{array}$	$\rho = \theta$ -0.057 -0.034 -0.022 -0.016 -0.013 root m $\rho = \theta$ 0.091	$\begin{array}{c} bias \\ \hline bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ -0.027 \\ -0.019 \\ -0.014 \\ -0.012 \\ \hline ean square \\ \phi = 0.6 \\ \rho = 0.2 \\ 0.072 \end{array}$	p = 0.4 -0.026 -0.019 -0.015 -0.012 -0.011 p error $p = 0.4$ 0.054	$\rho = \theta$ -0.049 -0.030 -0.021 -0.016 -0.013 $\rho = \theta$ 0.076	$\phi = 0.2$ -0.040 -0.026 -0.018 -0.015 -0.013 $\phi = 0.2$ 0.065	= 0.8 $= 0.4$ $= 0.022$ $= 0.017$ $= 0.014$ $= 0.8$ $= 0.8$ $= 0.4$ $= 0.055$	$\rho = 0.6$ -0.024 -0.018 -0.015 -0.013 -0.012 $\rho = 0.6$ 0.044
T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25 T = 500 (s/n) <sup>-1</sup> 4 2	$\phi = 0.2$ $\rho = 0$ -0.028 -0.018 -0.012 -0.009 -0.007 $\phi = 0.2$ $\rho = 0$ 0.060 0.053	$\phi = 0$ -0.048 -0.029 -0.018 -0.013 -0.010 $\phi = 0$ 0.081 0.060	$\begin{array}{c} \textbf{0.4} \\ \textbf{\rho} = \textbf{0.2} \\ -0.027 \\ -0.019 \\ -0.013 \\ -0.011 \\ -0.009 \\ \hline \textbf{0.4} \\ \textbf{\rho} = \textbf{0.2} \\ 0.059 \\ 0.052 \end{array}$	p = 0 -0.057 -0.034 -0.022 -0.016 -0.016 -0.013 <b>root m</b> $p = 0$ 0.091 0.063	$\begin{array}{c} bias \\ \hline bias \\ \phi = 0.6 \\ \rho = 0.2 \\ -0.042 \\ -0.027 \\ -0.019 \\ -0.014 \\ -0.012 \\ \hline eean square \\ \phi = 0.6 \\ \rho = 0.2 \\ 0.072 \\ 0.055 \end{array}$	p = 0.4 -0.026 -0.019 -0.015 -0.012 -0.011 e error $p = 0.4$ 0.054 0.047	$\rho = 0$ -0.049 -0.030 -0.021 -0.016 -0.013 $\rho = 0$ 0.076 0.076	$\phi = 0.2$ -0.040 -0.026 -0.018 -0.015 -0.013 $\phi = 0.2$ 0.065 0.048	= 0.8 $p = 0.4$ -0.033 -0.022 -0.017 -0.014 -0.013 $= 0.8$ $p = 0.4$ 0.055 0.043	$\rho = 0.6$ -0.024 -0.018 -0.015 -0.013 -0.012 $\rho = 0.6$ 0.044 0.038
T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25 T = 500 (s/n) <sup>-1</sup> 4 2 1	$\phi = 0.2$ $\rho = 0$ -0.028 -0.018 -0.012 -0.009 -0.007 $\phi = 0.2$ $\rho = 0$ 0.060 0.053 0.049	$\phi = \frac{\phi}{\rho = 0}$ -0.048 -0.029 -0.018 -0.013 -0.010 $\phi = \frac{\phi}{\rho = 0}$ -0.081 -0.060 -0.051	$\begin{array}{c} 0.4 \\ \rho = 0.2 \\ -0.027 \\ -0.019 \\ -0.013 \\ -0.011 \\ -0.009 \\ \hline 0.04 \\ \rho = 0.2 \\ 0.052 \\ 0.052 \\ 0.048 \end{array}$	p = 0 -0.057 -0.034 -0.022 -0.016 -0.013 <b>root m</b> $p = 0$ 0.091 0.063 0.051	$\begin{array}{c} bias \\ \hline bias \\ \hline \phi = 0.6 \\ \hline \rho = 0.2 \\ -0.042 \\ -0.019 \\ -0.019 \\ -0.014 \\ -0.012 \\ \hline ean square \\ \hline \phi = 0.6 \\ \hline \rho = 0.2 \\ 0.072 \\ 0.055 \\ 0.047 \end{array}$	$\rho = 0.4$ -0.026 -0.019 -0.015 -0.012 -0.011 error $\rho = 0.4$ 0.054 0.047	$\rho = 0$ -0.049 -0.030 -0.021 -0.016 -0.013 -0.016 -0.013 -0.053 0.042	$\phi = 0.2$ -0.040 -0.026 -0.018 -0.015 -0.013 $\phi = 0.2$ 0.065 0.048 0.039	= 0.8 $= 0.4$ $= 0.033$ $= 0.022$ $= 0.017$ $= 0.014$ $= 0.013$ $= 0.8$ $= 0.4$ $= 0.45$ $= 0.043$ $= 0.038$	<i>ρ</i> = 0.6 -0.024 -0.018 -0.015 -0.013 -0.012 <i>ρ</i> = 0.6 0.044 0.038 0.036
T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25 $T = 500$ (s/n) <sup>-1</sup> 4 2 1 0.5	$\phi = 0.2$ $\rho = 0$ -0.028 -0.018 -0.012 -0.009 -0.007 $\phi = 0.2$ $\rho = 0$ 0.060 0.053 0.049 0.049	$\phi = 0$ -0.048 -0.029 -0.018 -0.013 -0.010 $\phi = 0$ 0.081 0.060 0.051 0.048	$\begin{array}{c} 0.4 \\ \rho = 0.2 \\ -0.027 \\ -0.019 \\ -0.013 \\ -0.011 \\ -0.009 \\ \hline 0.011 \\ -0.009 \\ \hline 0.059 \\ 0.052 \\ 0.048 \\ 0.046 \end{array}$	p = 0 -0.057 -0.034 -0.022 -0.016 -0.013 <i>root m</i> $p = 0$ 0.091 0.063 0.051 0.045	$bias \phi = 0.6 \rho = 0.2 -0.042 -0.019 -0.014 -0.014 -0.014 -0.014 -0.014 -0.014 -0.015 0.047 0.055 0.047 0.047 0.047 0.047 0.047 0.047 0.047 0.047 -0.042 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.019 -0.014 -0.019 -0.014 -0.017 -0.014 -0.014 -0.014 -0.014 -0.017 -0.014 -0.014 -0.017 -0.014 -0.014 -0.017 -0.014 -0.017 -0.014 -0.017 -0.014 -0.017 -0.014 -0.017 -0.017 -0.014 -0.017 -0.014 -0.017 -0.014 -0.017 -0.014 -0.017 -0.014 -0.017 -0.014 -0.017 -0.014 -0.017 -0.017 -0.014 -0.017$	p = 0.4 -0.026 -0.019 -0.015 -0.012 -0.011 eerror $p = 0.4$ 0.054 0.047 0.044	p = 0 -0.049 -0.030 -0.021 -0.016 -0.013 $p = 0$ 0.076 0.053 0.042 0.037	$\phi = 0.2$ -0.040 -0.026 -0.018 -0.015 -0.013 $\phi = 0.2$ 0.065 0.048 0.039 0.036	$\begin{array}{c} \textbf{0.8} \\ \textbf{\rho} = \textbf{0.4} \\ -0.033 \\ -0.022 \\ -0.017 \\ -0.014 \\ -0.013 \end{array}$	<i>ρ</i> = 0.6 -0.024 -0.018 -0.015 -0.013 -0.012 <i>ρ</i> = 0.6 0.044 0.038 0.036
T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25 T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5 0.5 0.25	$\phi = 0.2$ $\rho = 0$ -0.028 -0.018 -0.012 -0.009 -0.007 $\phi = 0.2$ $\rho = 0$ 0.060 0.053 0.049 0.048 0.047	$\phi = 0$ -0.048 -0.029 -0.018 -0.013 -0.010 -0.010 -0.010 -0.010 -0.081 0.060 0.051 0.048 0.0448 -0.048 -0.	$\begin{array}{c} 0.4 \\ \rho = 0.2 \\ -0.027 \\ -0.019 \\ -0.013 \\ -0.011 \\ -0.009 \\ \hline 0.059 \\ 0.059 \\ 0.052 \\ 0.048 \\ 0.046 \\ 0.046 \\ 0.046 \end{array}$	p = 0 -0.057 -0.034 -0.022 -0.016 -0.013 root m $p = 0$ 0.091 0.063 0.051 0.045 0.045	bias $\phi = 0.6$ $\rho = 0.2$ -0.042 -0.027 -0.014 -0.012 ean square $\phi = 0.6$ $\rho = 0.2$ 0.072 0.055 0.047 0.044 0.044	p = 0.4 -0.026 -0.019 -0.015 -0.012 -0.011 2 error $p = 0.4$ 0.054 0.047 0.044 0.043 0.043	p = 0 -0.049 -0.030 -0.021 -0.016 -0.013 $p = 0$ 0.076 0.053 0.042 0.034	$\phi = 0.2$ -0.040 -0.026 -0.013 -0.013 -0.013 -0.013 -0.013 -0.013 -0.05 0.048 0.039 0.036 0.034	= 0.8 $p = 0.4$ $-0.033$ $-0.022$ $-0.014$ $-0.013$ $= 0.8$ $p = 0.4$ $0.055$ $0.043$ $0.038$ $0.035$ $0.035$	<b>ρ = 0.6</b> -0.024 -0.018 -0.015 -0.013 -0.012 <b>ρ = 0.6</b> 0.044 0.038 0.036 0.034
T = 500 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25 $T = 500$ (s/n) <sup>-1</sup> 4 2 1 0.5 0.5 0.25	$\phi = 0.2$ $\rho = 0$ -0.028 -0.012 -0.009 -0.007 $\phi = 0.2$ $\rho = 0$ 0.060 0.053 0.049 0.048 0.047	$\phi = \frac{\phi = \theta}{-0.048}$ -0.029 -0.013 -0.010 $\phi = \frac{\phi = \theta}{-0.081}$ 0.060 0.051 0.048 0.046	$\begin{array}{c} \textbf{a}\textbf{n}\textbf{b}\textbf{r} \\ \textbf{a}\textbf{b}\textbf{r} \\ \textbf{p} = \textbf{0}.2 \\ -0.027 \\ -0.019 \\ -0.013 \\ -0.011 \\ -0.009 \\ \hline \textbf{0}.009 \\ \hline \textbf{0}.$	p = 0 -0.057 -0.034 -0.022 -0.013 root m $p = 0$ 0.063 0.051 0.043 autoexteen set in the set of	bias $\phi = 0.6$ $\rho = 0.2$ -0.042 -0.019 -0.019 -0.019 -0.012 ean square $\phi = 0.6$ $\rho = 0.2$ 0.072 0.012 0.025 0.047 0.044 0.044 0.042	p = 0.4 -0.026 -0.019 -0.015 -0.015 -0.011 -0.011 2 error $p = 0.4$ 0.054 0.047 0.044 0.043 0.042	$\rho = 0$ -0.049 -0.030 -0.021 -0.013 -0.013 -0.013 -0.076 0.053 0.042 0.037 0.034	$\phi = 0.2$ -0.040 -0.026 -0.018 -0.015 -0.013 $\phi = 0.2$ 0.065 0.048 0.039 0.036 0.034	$ \begin{array}{c} \textbf{0.8} \\ \textbf{\rho} = \textbf{0.4} \\ -0.033 \\ -0.022 \\ -0.014 \\ -0.013 \\ \hline \textbf{\rho} = \textbf{0.4} \\ 0.055 \\ 0.043 \\ 0.038 \\ 0.035 \\ 0.034 \\ \end{array} $	$\begin{array}{c} \rho = 0.6 \\ -0.024 \\ -0.018 \\ -0.015 \\ -0.013 \\ -0.012 \end{array}$ $\begin{array}{c} \rho = 0.6 \\ 0.044 \\ 0.038 \\ 0.036 \\ 0.034 \\ 0.033 \end{array}$
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Table 3: Single break point, heteroskedastic case, N=30: bias and RMSE of parameters

The Table reports Monte Carlo bias and RMSE statistics concerning the estimation of the common factor ( $\phi$ ) and idiosyncratic ( $\rho$ ) autoregressive parameter. Results are reported for various values of the common factor autoregressive parameter  $\phi$  (0, 2, 0, 4, 0, 6, 0.8), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0, 2, 0, 4, 0, 6), assuming  $\phi > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 30, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved autoregressive factor and known single break point.

<i>Tuble</i> 4. 1w	о бгеак ро	inis, neier	oskeaasuc	case, N	50: Dias an	a KMSE OJ	paramete	ers		
					N=30					
L			autore	gressive c	ommon fac	ctor param	eter ø			
					bias					
T = 100	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	= 0.8	
$(s/n)^{-1}$	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0$	$\rho = 0$	$\rho = \theta$	$\rho = 0$	$\rho = 0$	$\rho = \theta$
4	-0.065	-0.096	-0.068	-0.115	-0.094	-0.070	-0.128	-0.116	-0.102	-0.082
2	0.054	0.076	0.060	0.002	0.094	0.072	0.126	0.100	0.005	0.082
1	-0.034	-0.070	-0.004	-0.092	-0.031	-0.072	-0.100	-0.100	-0.095	-0.088
1	-0.048	-0.000	-0.061	-0.078	-0.075	-0.0/1	-0.094	-0.092	-0.090	-0.087
0.5	-0.046	-0.061	-0.059	-0.072	-0.070	-0.069	-0.089	-0.088	-0.087	-0.087
0.25	-0.044	-0.058	-0.057	-0.069	-0.068	-0.068	-0.086	-0.085	-0.085	-0.085
				root m	ean square	error ?				
T = 100	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	= 0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0$	$\rho = \theta$	$\rho = \theta$	$\rho = 0$	$\rho = \theta$	$\rho = 0$
4	0.138	0.168	0.137	0.191	0.162	0.133	0.201	0.184	0.163	0.136
2	0.127	0.146	0.132	0.161	0.148	0.136	0.171	0.162	0.155	0.145
1	0.122	0.135	0.130	0.145	0.141	0.136	0.154	0.152	0.149	0.144
0.5	0.121	0.131	0.128	0.138	0.136	0.134	0.147	0.146	0.145	0.145
0.25	0.119	0.127	0.120	0.134	0.133	0.133	0.143	0.143	0.142	0.142
0.23	0.117	0.127	0.127	0.154	0.155	0.155	0.145	0.145	0.172	0.142
<u> </u>				autoregi	essive para	imeier p				
-	, <u>.</u>		<u> </u>	1	bias			· ·		
T = 100	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	- 0.8	
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = \theta$	$\rho = \theta$	$\rho = \theta$	$\rho = \theta$	$\rho = \theta$	$\rho = \theta$
4	-0.020	-0.024	-0.032	-0.026	-0.035	-0.049	-0.029	-0.038	-0.050	-0.062
2	-0.021	-0.025	-0.035	-0.027	-0.036	-0.047	-0.027	-0.037	-0.051	-0.062
1	-0.020	-0.022	-0.038	-0.024	-0.037	-0.051	-0.028	-0.039	-0.048	-0.064
0.5	-0.021	-0.020	-0.033	-0.027	-0.039	-0.048	-0.030	-0.037	-0.053	-0.059
0.25	-0.020	-0.022	-0.035	-0.026	-0.037	-0.048	-0.025	-0.042	-0.052	-0.061
0.20	0.020	0.022	0.000	root m	aan sauar	arror	0.020	0.0.12	0.002	0.001
T = 100	4 - 0 2	4 -	- 0 4	1001 m	$\frac{1}{4} = 0.6$	enor		4 -		
I = I00	$\phi = 0.2$	φ =	0.4	0	$\phi = 0.0$	0	0	φ =	0.8	0
(s/n) <sup>-1</sup>	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	$\rho = 0$	$\rho = 0$	$\rho = 0$	$\rho = 0$	$\rho = 0$	$\rho = 0$
4	0.105	0.105	0.107	0.107	0.110	0.116	0.107	0.113	0.119	0.124
2	0.104	0.105	0.109	0.107	0.113	0.116	0.105	0.114	0.119	0.124
1	0.104	0.103	0.114	0.107	0.115	0.118	0.110	0.114	0.118	0.127
0.5	0.103	0.105	0.111	0.108	0.115	0.117	0.108	0.113	0.121	0.122
0.25	0.103	0.105	0.111	0.107	0.111	0.117	0.105	0.114	0.122	0.122
			autore	gressive c	ommon fac	tor param	eter ø			
				0	bias					
T = 500	$\phi = 0.2$	<i>d</i> -	- 0 1		$\phi = 0.6$			<i>d</i> -	- 0.8	
1 - 300	$\psi = 0.2$	$\varphi = 0$	0.4	a = 0	$\varphi = 0.0$	a = 0.4	a = 0	$\varphi = 0.2$	a = 0.4	a = 0.6
(5/1)	p = 0	p = 0	p = 0.2	p - 0	p = 0.2	p = 0.4	p = 0	p = 0.2	p = 0.4	p = 0.0
4	-0.032	-0.032	-0.030	-0.004	-0.048	-0.032	-0.034	-0.045	-0.038	-0.028
2	-0.022	-0.032	-0.022	-0.041	-0.033	-0.025	-0.036	-0.031	-0.027	-0.023
1	-0.016	-0.022	-0.017	-0.029	-0.025	-0.021	-0.026	-0.024	-0.022	-0.020
0.5	-0.014	-0.017	-0.014	-0.023	-0.021	-0.019	-0.021	-0.020	-0.019	-0.018
0.25	-0.012	-0.014	-0.013	-0.019	-0.019	-0.018	-0.019	-0.018	-0.018	-0.017
				root m	ean square	error				
T = 500	$\phi = 0.2$	φ=	= 0.4		$\phi = \overline{0.6}$			φ =	- 0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.065	0.086	0.061	0.100	0.079	0.060	0.084	0.072	0.063	0.050
2	0.057	0.063	0.053	0.071	0.061	0.052	0.060	0.054	0.050	0.044
1	0.052	0.053	0.050	0.057	0.053	0.049	0.048	0.046	0.044	0.041
0.5	0.050	0.049	0.047	0.051	0.049	0.047	0.043	0.041	0.041	0.039
0.25	0.050	0.047	0.047	0.048	0.047	0.046	0.040	0.039	0.039	0.038
0.45	0.050	0.047	0.077	autona	accina nam	0.0+0	0.040	0.057	0.057	0.050
<u> </u>				autoregi	bing	imeier p				
	/ <u></u>		<u> </u>	1	DIAS			· ·		
T = 500	$\phi = 0.2$	φ =	= 0.4	-	$\phi = 0.6$			φ =	- 0.8	
(s/n) <sup>-1</sup>	$\rho = 0$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	-0.006	-0.004	-0.007	-0.005	-0.007	-0.009	-0.005	-0.009	-0.010	-0.012
2	-0.003	-0.005	-0.006	-0.004	-0.008	-0.009	-0.005	-0.008	-0.008	-0.012
1	-0.004	-0.006	-0.008	-0.006	-0.007	-0.009	-0.009	-0.009	-0.011	-0.011
0.5	-0.006	-0.003	-0.007	-0.005	-0.007	-0.011	-0.006	-0.007	-0.011	-0.013
0.25	-0.005	-0.004	-0.007	-0.006	-0.008	-0.011	-0.006	-0.008	-0.010	-0.011
				root w	oan sauar	error				
T - 500	4 - 0 2	<b>1</b> -	- 0 4	1001 M	an synure			4 -	- 0.9	
1 - 300	$\varphi = 0.2$	φ=	- 0.4		$\psi = 0.0$	0 4		φ =	- 0.0	0 /
$(s/n)^{-1}$	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.046	0.046	0.043	0.044	0.046	0.044	0.046	0.044	0.044	0.040
2	0.044	0.045	0.045	0.046	0.045	0.043	0.046	0.046	0.042	0.042
1	0.045	0.045	0.045	0.047	0.045	0.043	0.047	0.044	0.044	0.039
0.5	0.046	0.044	0.046	0.045	0.045	0.044	0.046	0.045	0.044	0.041
0.25	0.046	0.045	0.045	0.046	0.045	0.044	0.045	0.046	0.043	0.040

#### Table 4: Two break points, heteroskedastic case, N=30: bias and RMSE of parameters

The Table reports Monte Carlo bias and RMSE statistics concerning the estimation of the common factor ( $\phi$ ) and idiosyncratic ( $\rho$ ) autoregressive parameter. Results are reported for various values of the common factor autoregressive parameter  $\phi$  (0, 2, 0, 4, 0, 6, 0.8), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0, 2, 0, 4, 0, 6), assuming  $\phi > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 30, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved autoregressive factor and known break points.

Table 5: S	Single and	multiple l	break point	ts, hetero:	skedastic c	ase, N=30:	Monte C	arlo Theil	and correl	ation statis
				~~~~~~	N=30	sina faatau				
				1-h	reak noint	sive jucior case				
				10.	Theil index	r				
T = 100	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ=	= 0.8	
(s/n) <sup>-1</sup>	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.195	0.195	0.197	0.199	0.201	0.208	0.224	0.225	0.229	0.239
2	0.151	0.156	0.157	0.169	0.170	0.174	0.208	0.208	0.211	0.216
1	0.122	0.131	0.132	0.151	0.151	0.154	0.198	0.199	0.200	0.203
0.5	0.103	0.115	0.116	0.140	0.140	0.142	0.193	0.193	0.194	0.195
0.25	0.092	0.106	0.107	0.134	0.134	0.135	0.190	0.190	0.190	0.191
				corre	lation coef	ficient				
T = 100	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			<i>φ</i> =	= 0.8	
(s/n)-1	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.932	0.934	0.933	0.936	0.935	0.929	0.932	0.931	0.928	0.919
2	0.961	0.961	0.960	0.957	0.957	0.954	0.945	0.945	0.943	0.939
1	0.977	0.975	0.974	0.968	0.968	0.967	0.952	0.952	0.951	0.949
0.5	0.984	0.982	0.982	0.974	0.974	0.975	0.930	0.930	0.930	0.934
0.25	0.988	0.985	0.985	0.977	0.977	0.977	0.958	0.958	0.958	0.957
T - 500	4-02	4 -	- 0 1		<u>1 neu inde</u>	τ.	1	J -	- 0 8	
1 - 300	$\varphi = 0.2$	$\varphi = 0$	-0.4	a = 0	$\varphi = 0.0$	a = 0.4	0 - 0	$\phi = 0.2$	-0.0	a = 0.6
(s/n) ·	p = 0	p = 0	p = 0.2	p = 0 0.157	p = 0.2	p = 0.4	p = 0	p = 0.2	p = 0.4	p = 0.0
2	0.178	0.170	0.175	0.137	0.100	0.108	0.141	0.142	0.148	0.102
2	0.150	0.120	0.120	0.120	0.122	0.120	0.117	0.110	0.122	0.131
0.5	0.097	0.075	0.076	0.095	0.097	0.100	0.003	0.103	0.105	0.098
0.5	0.074	0.073	0.070	0.030	0.030	0.083	0.093	0.094	0.095	0.098
0.23	0.058	0.002	0.002	0.070	0.070	Giorna di Contenti	0.000	0.089	0.009	0.091
T = 500	4 - 0.2	<i>d</i> -	- 0 4	corre	$\frac{1}{4} - 0.6$	ncieni		<i>d</i> -	- 0.9	
I = 300	$\varphi = 0.2$	$\varphi = 0$	-0.4	a = 0	$\varphi = 0.0$	a = 0.4	a = 0	$\varphi = 0.2$	-0.0	a = 0.6
(3/11)	p = 0	p = 0	p = 0.2	p = 0	p = 0.2	p = 0.4	p = 0	p = 0.2	p = 0.4	p = 0.0
2	0.940	0.945	0.944	0.935	0.955	0.948	0.908	0.907	0.903	0.930
1	0.983	0.984	0.983	0.985	0.985	0.983	0.986	0.985	0.984	0.982
0.5	0.903	0.991	0.990	0.991	0.990	0.990	0.989	0.989	0.988	0.987
0.5	0.994	0.994	0.994	0.993	0.993	0.993	0.990	0.990	0.990	0.989
0.20	0.774	0.774	0.774	2_h	roak noint	case	0.770	0.770	0.770	0.707
				20	Theil inde	r				
T = 100	$\phi = 0.2$	φ=	= 0.4		$\phi = 0.6$	•		ф =	= 0.8	
$(s/n)^{-1}$	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.204	0.209	0.211	0.221	0.223	0.229	0.267	0.268	0.270	0.278
2	0.162	0.173	0.174	0.195	0.196	0.199	0.254	0.254	0.256	0.260
1	0.136	0.151	0.152	0.180	0.180	0.182	0.246	0.246	0.247	0.249
0.5	0.119	0.138	0.139	0.171	0.171	0.172	0.242	0.242	0.243	0.244
0.25	0.110	0.131	0.131	0.166	0.166	0.167	0.240	0.240	0.241	0.241
				corre	lation coef	ficient				
T=100	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	= 0.8	
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.923	0.922	0.920	0.916	0.915	0.909	0.890	0.889	0.886	0.877
2	0.953	0.949	0.948	0.938	0.937	0.935	0.904	0.904	0.902	0.898
1	0.968	0.963	0.962	0.949	0.948	0.947	0.911	0.911	0.910	0.908
0.5	0.976	0.970	0.970	0.954	0.954	0.954	0.915	0.915	0.914	0.913
0.25	0.980	0.974	0.973	0.957	0.957	0.957	0.917	0.917	0.917	0.916
					Theil index	r				
T = 500	$\phi = 0.2$	φ=	= 0.4		$\phi = 0.6$			φ =	= <i>0.8</i>	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = \theta.2$	$\rho = \theta$	$\rho = \theta.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.185	0.178	0.180	0.166	0.168	0.176	0.157	0.158	0.164	0.176
2	0.139	0.136	0.138	0.132	0.133	0.139	0.136	0.137	0.140	0.148
1	0.109	0.109	0.110	0.110	0.111	0.114	0.124	0.124	0.126	0.131
0.5	0.089	0.092	0.093	0.097	0.097	0.099	0.117	0.117	0.118	0.121
0.25	0.077	0.082	0.082	0.089	0.090	0.091	0.113	0.114	0.114	0.115
				corre	lation coef	ficient				
$T = \overline{500}$	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	= 0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = \theta.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.935	0.940	0.939	0.949	0.948	0.942	0.958	0.957	0.954	0.945
2	0.963	0.965	0.964	0.969	0.968	0.965	0.970	0.969	0.967	0.963
1	0.978	0.979	0.978	0.979	0.979	0.977	0.976	0.975	0.975	0.972
0.5	0.986	0.985	0.985	0.984	0.984	0.983	0.979	0.979	0.978	0.977
0 25	0.080	0.080	0 080	0.087	0.087	0.086	0.080	0.080	0.080	0.070

The Table reports Monte Carlo *Theil index and correlation coefficient* statistics concerning the estimation of the unobserved common factor component. Results are reported for various values of the common factor autoregressive parameter  $\phi$  (0.2, 0.4, 0.6, 0.8), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0.2, 0.4, 0.6), assuming  $\phi > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 30, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved autoregressive factor and known break points.

Table 6: S	Single and	multiple l	break point	ts, hetero.	skedastic c	ase, N=30:	Monte C	arlo Theil	and correl	ation statis
					N=30					
				<i>comm</i>	on break p	orocess				
				1-0	reak point Thail inda	case				
T - 100	1 - 0.2	1 -	- 0.4		1 neu inae.	c	I	1 -	- 0.0	
I = 100	$\varphi = 0.2$	$\varphi = 0$	= 0.4	a = 0	$\varphi = 0.0$	a = 0.4	0 - 0	$\varphi = 0.2$	= 0.8	a = 0.6
(s/n) -	p - v	p - 0	p = 0.2	p - 0	p = 0.2	p = 0.4	p - 0	p = 0.2	p = 0.4	p = 0.0
4	0.029	0.037	0.037	0.055	0.055	0.056	0.105	0.105	0.106	0.107
2	0.028	0.030	0.037	0.055	0.055	0.055	0.105	0.105	0.105	0.100
1	0.028	0.030	0.030	0.055	0.055	0.055	0.105	0.105	0.105	0.105
0.5	0.028	0.030	0.030	0.055	0.055	0.055	0.105	0.105	0.105	0.105
0.23	0.028	0.050	0.050	0.033	0.033	0.033	0.105	0.103	0.105	0.103
T = 100	1 - 0.2	1 -	- 0.4	corre	lation coef	icient	I	1 -	- 0.0	
I = 100	$\varphi = 0.2$	$\varphi = 0$	= 0.4	a = 0	$\varphi = 0.0$	a = 0.4	0 - 0	$\varphi = 0.2$	= 0.8	a = 0.6
(s/n) ·	p - v	p - 0	p = 0.2	p - 0	p = 0.2	p = 0.4	p - 0	p = 0.2	p = 0.4	p = 0.0
4	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
2	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
1	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
0.5	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
0.25	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
<b>T T A A A</b>	1 0 0	,	0.4		1 heil inde:	r	<u>r</u>		0.0	
T = 500	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$	A /		φ =	= 0.8	
(s/n)-1	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.013	0.017	0.017	0.025	0.025	0.026	0.048	0.048	0.049	0.049
2	0.013	0.017	0.017	0.025	0.025	0.026	0.048	0.048	0.048	0.048
1	0.013	0.016	0.017	0.025	0.025	0.025	0.048	0.048	0.048	0.048
0.5	0.013	0.017	0.017	0.025	0.025	0.025	0.048	0.048	0.048	0.048
0.25	0.013	0.016	0.017	0.025	0.025	0.025	0.048	0.048	0.048	0.048
				corre	lation coe <u>f</u>	ficient				
T = 500	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	= 0.8	
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
2	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
1	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
0.5	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
0.25	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
				2-b	reak point	case				
					Theil inde:	r				
T = 100	$\phi = 0.2$	φ=	= 0.4		$\phi = 0.6$			φ=	= 0.8	
(s/n) <sup>-1</sup>	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.040	0.052	0.052	0.076	0.077	0.078	0.141	0.141	0.142	0.144
2	0.039	0.051	0.052	0.076	0.076	0.076	0.141	0.141	0.141	0.142
1	0.039	0.051	0.051	0.075	0.075	0.076	0.141	0.141	0.141	0.141
0.5	0.038	0.051	0.051	0.075	0.075	0.075	0.141	0.141	0.141	0.141
0.25	0.038	0.051	0.051	0.075	0.075	0.075	0.141	0.141	0.141	0.141
				corre	lation coef	ficient				
T = 100	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	= 0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.997	0.995	0.995	0.988	0.988	0.987	0.957	0.958	0.957	0.955
2	0.997	0.995	0.995	0.988	0.988	0.988	0.958	0.957	0.958	0.957
1	0.997	0.995	0,995	0.988	0.988	0,988	0.958	0.958	0.957	0.958
0.5	0.997	0.995	0,995	0.988	0.988	0,988	0.958	0.957	0.958	0.958
0.25	0.997	0.995	0,995	0.988	0.988	0,988	0.958	0.958	0.958	0.958
					Theil inde	r				0.700
T = 500	$\phi = 0.2$	<i>ф</i> -	= 0 4		$\phi = 0.6$	•	1	<i>d</i> -	= 0.8	
(s/n)-1	$\varphi = 0.2$	$\phi = 0$	0 = 0.7	$\rho = 0$	$\varphi = 0.0$	$\rho = 0.4$	$\rho = 0$	$\varphi = 0.2$	0 = 0.4	$\rho = 0.6$
4	$\frac{p}{0.025}$	p = 0 0.030	0.030	0.030	0.030	0.040	p = 0 0.070	0.070	0.070	0.071
7	0.025	0.030	0.030	0.039	0.039	0.040	0.070	0.070	0.070	0.070
	0.025	0.030	0.030	0.039	0.039	0.040	0.070	0.070	0.070	0.070
<u> </u>	0.025	0.029	0.030	0.039	0.039	0.039	0.070	0.070	0.070	0.070
0.5	0.025	0.029	0.029	0.039	0.039	0.039	0.070	0.070	0.070	0.070
0.23	0.023	0.029	0.029	0.039	0.039	0.039	0.070	0.070	0.070	0.070
<b>T T A A A</b>	1	,	0.4	corre	uation coef	ncient	1		0.0	
1 = 500	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$		-	φ =	= 0.8	-
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.998	0.997	0.997	0.996	0.996	0.996	0.990	0.990	0.990	0.990
2	0.998	0.998	0.997	0.996	0.996	0.996	0.990	0.990	0.990	0.990
1	0.998	0.998	0.998	0.996	0.996	0.996	0.990	0.990	0.990	0.990
0.5	0.998	0.998	0.998	0.996	0.996	0.996	0.990	0.990	0.990	0.990
0.25	0.998	0.998	0.998	0.996	0.996	0.996	0.990	0.990	0.990	0.990

The Table reports Monte Carlo *RMSE, Theil index and correlation coefficient* statistics, concerning the estimation of the unobserved common break process component. Results are reported for various values of the common factor autoregressive parameter  $\phi$  (0.2, 0.4, 0.6, 0.8), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0.2, 0.4, 0.6), assuming  $\phi > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 30, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved autoregressive factor and known break points.

Table 7: No s	structural l	break, hete	eroskedasti	c case: bia	s of autore	egressive co	ommon fa	ctor param	eter ø	
			autore	gressive c	ommon fac	ctor param	eter ø			
7 100	1 0.0	,	0.4	<i>l</i>	ias N = 3	5			0.0	
T = 100	$\phi = 0.2$	$\phi = 0$	= 0.4	a <b>–</b> 0	$\phi = 0.6$	a = 0.4	a <b>=</b> 0	$\phi = 0.2$	= 0.8	0 - 0 6
(5/11)	p = 0	p = 0	-0.101	p = 0	p = 0.2	p = 0.4	-0.230	p = 0.2	p = 0.4	-0.094
2	-0.073	-0.125	-0.075	-0.154	-0.115	-0.075	-0.146	-0.122	-0.142	-0.075
1	-0.049	-0.081	-0.055	-0.098	-0.078	-0.058	-0.096	-0.083	-0.073	-0.058
0.5	-0.035	-0.055	-0.041	-0.067	-0.056	-0.044	-0.067	-0.060	-0.054	-0.050
0.25	-0.029	-0.041	-0.033	-0.049	-0.043	-0.037	-0.052	-0.049	-0.046	-0.043
				b	ias N=1	0				
T = 100	$\phi = 0.2$	φ=	0.4		$\phi = 0.6$			φ =	<i>0.8</i>	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	-0.072	-0.126	-0.072	-0.155	-0.113	-0.069	-0.150	-0.122	-0.098	-0.066
2	-0.046	-0.083	-0.053	-0.099	-0.079	-0.057	-0.098	-0.085	-0.0/1	-0.057
1	-0.032	-0.055	-0.042	-0.067	-0.056	-0.045	-0.070	-0.065	-0.057	-0.051
0.5	-0.023	-0.041	-0.034	-0.030	-0.043	-0.039	-0.034	-0.031	-0.048	-0.043
0.25	-0.010	-0.055	-0.027	-0.041 h	ias N = 1	-0.050	-0.0+0	-0.045	-0.0+5	-0.042
T = 100	$\phi = 0.2$	φ =	0.4	<i>v</i>	$\phi = 0.6$	-		φ =	- 0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	-0.058	-0.098	-0.056	-0.117	-0.086	-0.050	-0.118	-0.099	-0.081	-0.056
2	-0.037	-0.063	-0.042	-0.077	-0.060	-0.044	-0.082	-0.071	-0.064	-0.052
1	-0.030	-0.046	-0.037	-0.051	-0.045	-0.038	-0.061	-0.057	-0.053	-0.048
0.5	-0.023	-0.035	-0.030	-0.040	-0.036	-0.033	-0.051	-0.048	-0.047	-0.045
0.25	-0.019	-0.030	-0.028	-0.033	-0.032	-0.030	-0.045	-0.044	-0.044	-0.043
				b	ias N = 5	0				
T = 100	$\phi = 0.2$	$\phi = 0$	= 0.4	a <b>–</b> 0	$\phi = 0.6$	a = 0.4	a <b>=</b> 0	$\phi = 0.2$	= 0.8	0 - 0 6
(s/n)	p - 0	p - 0	p = 0.2	p = 0	p = 0.2	p = 0.4	p = 0	p = 0.2	p = 0.4	p = 0.0
2	-0.027	-0.040	-0.027	-0.038	-0.043	-0.028	-0.002	-0.034	-0.047	-0.039
1	-0.019	-0.027	-0.024	-0.035	-0.033	-0.031	-0.043	-0.042	-0.042	-0.040
0.5	-0.017	-0.024	-0.023	-0.032	-0.031	-0.030	-0.040	-0.039	-0.039	-0.039
0.25	-0.016	-0.023	-0.022	-0.029	-0.029	-0.029	-0.038	-0.038	-0.038	-0.038
				l	bias N=:	5				
T = 500	$\phi = 0.2$	φ =	0.4		$\phi = 0.6$			φ =	0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	-0.091	-0.165	-0.087	-0.208	-0.144	-0.080	-0.190	-0.149	-0.112	-0.070
2	-0.058	-0.104	-0.057	-0.127	-0.089	-0.052	-0.110	-0.088	-0.067	-0.045
1	-0.030	-0.002	-0.034	-0.074	-0.032	-0.031	-0.003	-0.030	-0.040	-0.028
0.25	-0.014	-0.020	-0.012	-0.024	-0.018	-0.013	-0.022	-0.019	-0.016	-0.013
0.20	0.01	0.020	0.012	h	ias $N=1$	0	0.022	0.017	0.010	0.010
T = 500	$\phi = 0.2$	φ =	0.4		$\phi = 0.6$			φ =	- <i>0.8</i>	
(s/n) <sup>-1</sup>	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	-0.058	-0.104	-0.055	-0.129	-0.090	-0.052	-0.110	-0.087	-0.066	-0.043
2	-0.034	-0.061	-0.034	-0.075	-0.053	-0.032	-0.062	-0.050	-0.040	-0.028
1	-0.019	-0.035	-0.020	-0.042	-0.031	-0.020	-0.036	-0.030	-0.024	-0.018
0.5	-0.011	-0.020	-0.013	-0.025	-0.019	-0.014	-0.022	-0.019	-0.016	-0.013
0.25	-0.007	-0.012	-0.008	-0.015	-0.013	-0.010	-0.015	-0.013	-0.012	-0.010
T - 500	4 - 0.2	<i>d</i> –	- 0 1	D	$\frac{1}{4} = 0.6$	3		<i>d</i> -	- 0.9	
1 - 300 (s/n) <sup>-1</sup>	$\varphi = 0.2$	$\varphi = 0$	a = 0.2	$\rho = 0$	$\varphi = 0.0$	$\rho = 0.4$	$\rho = 0$	$\varphi = 0.2$	a = 0.4	$\rho = 0.6$
4	-0.045	-0.078	-0.041	-0.094	-0.066	-0.038	-0.079	-0.063	-0.049	-0.032
2	-0.027	-0.046	-0.026	-0.054	-0.039	-0.024	-0.045	-0.037	-0.029	-0.022
1	-0.016	-0.026	-0.016	-0.031	-0.023	-0.016	-0.027	-0.023	-0.019	-0.015
0.5	-0.010	-0.015	-0.011	-0.018	-0.015	-0.011	-0.017	-0.015	-0.013	-0.011
0.25	-0.007	-0.010	-0.007	-0.013	-0.011	-0.009	-0.012	-0.011	-0.010	-0.009
				b	ias $N=5$	0				
T = 500	$\phi = 0.2$	φ =	0.4		$\phi = 0.6$	-		φ =	= 0.8	-
(s/n)-1	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	-0.019	-0.028	-0.015	-0.036	-0.026	-0.016	-0.031	-0.026	-0.021	-0.015
2	-0.012	-0.010	-0.010	-0.021	-0.010	-0.011	-0.019	-0.017	-0.015	-0.012
05	-0.009	-0.010	-0.007	-0.014	-0.009	-0.009	-0.014	-0.012	-0.011	-0.010
0.25	-0.006	-0.005	-0.004	-0.008	-0.007	-0.007	-0.009	-0.009	-0.009	-0.008

The Table reports Monte Carlo bias statistics concerning the estimation of the common factor ( $\phi$ ) autoregressive parameter. Results are reported for various values of the common factor autoregressive parameter  $\phi$  (0, 2, 0, 4, 0.6, 0.8), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0, 2, 0, 4, 0.6), assuming  $\phi > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 5, 10, 15, 50, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved autoregressive factor and no breaks.

able 8: No s	structural l	break, het	eroskedast	ic case: N	<i>1onte Carl</i>	o correlatio	on coeffic	ient statist	ic	
		<i>,</i>	autore	gressive a	common fa	ctor param	eter ø			
				, correlatio	on coefficie	nt N = 5	/			
T = 100	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	= 0.8	
$(s/n)^{-1}$	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.742	0.764	0.756	0.801	0.795	0.774	0.863	0.861	0.845	0.809
2	0.846	0.859	0.856	0.885	0.882	0.870	0.925	0.923	0.913	0.892
1	0.914	0.922	0.920	0.937	0.936	0.928	0.960	0.959	0.953	0.942
0.5	0.954	0.959	0.957	0.967	0.966	0.962	0.979	0.979	0.976	0.970
0.25	0.976	0.979	0.978	0.983	0.983	0.980	0.990	0.989	0.988	0.985
0.20				orrelatio	n coefficies	nt N = 10				
T = 100	$\phi = 0.2$	<i>d</i> =	= 0.4	onciano	$\phi = 0.6$			<i>d</i> =	= 0.8	
(s/n) <sup>-1</sup>	$\varphi = 0.2$	$\phi = 0$	a = 0.2	a = 0	$\varphi = 0.0$	a = 0.4	a = 0	a = 0.2	a = 0.4	a = 0.6
4	0.843	0.857	0.853	0.884	0.881	0.867	0.924	0.921	0.913	0.889
2	0.913	0.921	0.000	0.937	0.935	0.928	0.959	0.958	0.953	0.941
1	0.954	0.959	0.957	0.967	0.966	0.962	0.979	0.978	0.976	0.969
0.5	0.976	0.979	0.978	0.983	0.983	0.980	0.990	0.989	0.988	0.984
0.5	0.988	0.989	0.989	0.992	0.991	0.990	0.995	0.995	0.994	0.992
0.25	0.700	0.707	0.707	orrelatio	n coafficia	N = 15	0.775	0.775	0.774	0.772
T = 100	4 - 0.2	<i>d</i> -	- 0 4	orrelation		<i>u</i> 11–13		<i>h</i> -	- 0.9	
I = 100	$\varphi = 0.2$	$\varphi = 0$	-0.4	a = 0	$\psi = 0.0$	a = 0.4	a = 0	$\varphi = 0.2$	- 0.0	a = 0.6
(5/11)	p = 0	p = 0	p = 0.2	p = 0	p = 0.2	p = 0.4	p = 0	p = 0.2	p = 0.4	p = 0.0
2	0.000	0.046	0.094	0.918	0.910	0.900	0.947	0.943	0.939	0.922
2	0.939	0.940	0.944	0.937	0.930	0.950	0.972	0.972	0.908	0.939
1	0.908	0.972	0.971	0.978	0.977	0.974	0.980	0.965	0.964	0.979
0.5	0.964	0.960	0.965	0.989	0.966	0.987	0.993	0.993	0.992	0.969
0.23	0.992	0.993	0.993	0.994	0.994	0.993	0.990	0.990	0.990	0.993
T 100	1 0.2	,	0.1	orrelatio		u N – 30		1	0.0	
T = 100	$\phi = 0.2$	φ=	= 0.4	0	$\phi = 0.6$		0	φ=	= 0.8	
(s/n)	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.962	0.966	0.965	0.973	0.972	0.969	0.983	0.983	0.981	0.975
2	0.981	0.983	0.982	0.986	0.986	0.984	0.992	0.991	0.990	0.988
1	0.990	0.991	0.991	0.993	0.993	0.992	0.996	0.996	0.995	0.994
0.5	0.995	0.996	0.996	0.997	0.996	0.996	0.998	0.998	0.998	0.997
0.25	0.998	0.998	0.998	0.998	0.998	0.998	0.999	0.999	0.999	0.998
				correlatio	on coefficie	nt N = 5				
T = 500	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			<i>φ</i> =	= 0.8	
$(s/n)^{-1}$	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.750	0.772	0.765	0.811	0.806	0.786	0.877	0.873	0.859	0.827
2	0.849	0.864	0.860	0.891	0.888	0.875	0.933	0.930	0.922	0.901
1	0.916	0.925	0.922	0.941	0.939	0.931	0.965	0.963	0.958	0.947
0.5	0.955	0.960	0.959	0.969	0.968	0.964	0.982	0.981	0.979	0.972
0.25	0.977	0.979	0.979	0.984	0.984	0.981	0.991	0.990	0.989	0.986
			(	correlatio	n coefficie	nt N=10				
T = 500	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			<i>φ</i> =	= 0.8	
$(s/n)^{-1}$	$\rho = 0$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.849	0.864	0.860	0.891	0.887	0.874	0.933	0.930	0.922	0.901
2	0.916	0.925	0.922	0.941	0.939	0.931	0.965	0.963	0.959	0.947
1	0.955	0.960	0.959	0.969	0.968	0.964	0.982	0.981	0.979	0.972
0.5	0.977	0.979	0.979	0.984	0.984	0.981	0.991	0.990	0.989	0.986
0.25	0.988	0.990	0.989	0.992	0.992	0.991	0.995	0.995	0.995	0.993
			C	orrelatio	n coefficiei	nt N=15				
T = 500	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ =	= 0.8	
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0.891	0.903	0.899	0.923	0.920	0.911	0.954	0.952	0.946	0.931
2	0.941	0.948	0.946	0.959	0.958	0.952	0.976	0.975	0.972	0.964
1	0.969	0.973	0.972	0.979	0.978	0.975	0.988	0.987	0.986	0.981
0.5	0.984	0.986	0.986	0.989	0.989	0.987	0.994	0.994	0.993	0.991
0.25	0.992	0.993	0.993	0.995	0.994	0.994	0.997	0.997	0.996	0.995
			C	orrelatio	n coefficier	nt  N = 50				
T = 500	$\phi = 0.2$	φ =	= 0.4		$\phi = 0.6$			φ=	= 0.8	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$
4	0,963	0.968	0,966	0.975	0.974	0,970	0.985	0,985	0.983	0.978
2	0.981	0.983	0,983	0.987	0.987	0,985	0.993	0.992	0.991	0.989
1	0.991	0.992	0,991	0.994	0,993	0,992	0.996	0,996	0,996	0.994
0.5	0.995	0.996	0.996	0.997	0.997	0.996	0.998	0.998	0.998	0.997
0.25	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

The Table reports Monte Carlo *correlation coefficients* between the actual and estimated common factor. Results are reported for various values of the common factor autoregressive parameter  $\phi$  (0, 2, 0, 4, 0.6, 0.8), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0, 2, 0.4, 0.6), assuming  $\phi > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 5, 10, 15, 50, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved autoregressive factor and no breaks.

						aut	oregressiv	e paramet	er p	1	1				
T = 100	d = 0.2	<i>d</i> =	04		d = 0.6		DI	as d =	= 0.8				d = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	-0.013	-0.013	-0.029	-0.017	-0.026	-0.029	-0.018	-0.028	-0.038	-0.043	-0.021	-0.030	-0.037	-0.046	-0.060
2	-0.015	-0.015	-0.026	-0.022	-0.026	-0.034	-0.019	-0.027	-0.037	-0.046	-0.021	-0.029	-0.034	-0.048	-0.056
1	-0.015	-0.016	-0.027	-0.019	-0.021	-0.034	-0.018	-0.028	-0.037	-0.045	-0.021	-0.031	-0.033	-0.045	-0.058
0.5	-0.015	-0.015	-0.027	-0.018	-0.024	-0.036	-0.021	-0.030	-0.034	-0.050	-0.022	-0.028	-0.036	-0.044	-0.058
0.23	-0.014	-0.010	-0.023	-0.020	-0.027	-0.030	-0.022	-0.029	-0.030	-0.049	-0.020	-0.031	-0.037	-0.040	-0.037
T = 100	d = 0.2	<i>d</i> =	0.4		d = 0.6		on mean .	d =	= 0.8				d = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta.6$	$\rho = \theta.8$
4	0.102	0.103	0.106	0.100	0.102	0.101	0.101	0.106	0.109	0.106	0.105	0.108	0.110	0.110	0.112
2	0.103	0.104	0.105	0.105	0.107	0.104	0.104	0.105	0.109	0.109	0.104	0.106	0.106	0.111	0.107
1	0.102	0.103	0.105	0.103	0.101	0.109	0.102	0.103	0.108	0.107	0.104	0.107	0.103	0.106	0.110
0.5	0.104	0.101	0.105	0.102	0.106	0.105	0.103	0.110	0.107	0.113	0.106	0.106	0.107	0.105	0.109
0.23	0.102	0.103	0.104	0.105	0.100	0.107	0.104	e naramet	0.107	0.112	0.103	0.108	0.110	0.108	0.108
						uu	bi	as	πp			-	-	-	-
T = 500	d = 0.2	<i>d</i> =	0.4		d = 0.6			<i>d</i> =	= <i>0.8</i>				d = 1.0		,
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	-0.003	-0.002	-0.005	-0.004	-0.005	-0.006	-0.005	-0.004	-0.009	-0.007	-0.003	-0.005	-0.008	-0.009	-0.010
2	-0.001	-0.003	-0.003	-0.003	-0.006	-0.007	-0.005	-0.007	-0.007	-0.010	-0.003	-0.006	-0.007	-0.009	-0.010
0.5	-0.003	-0.002	-0.004	-0.004	-0.006	-0.008	-0.004	-0.006	-0.006	-0.009	-0.005	-0.006	-0.008	-0.009	-0.010
0.5	-0.002	-0.002	-0.008	-0.004	-0.006	-0.008	-0.003	-0.003	-0.007	-0.009	-0.002	-0.004	-0.003	-0.009	-0.010
0.25	0.005	0.004	0.000	0.005	0.005	0.000 r	oot mean s	auare erro	0.000	0.010	0.005	0.007	0.007	0.010	0.010
T = 500	d = 0.2	<i>d</i> =	0.4		d = 0.6			d =	0.8				d = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.045	0.045	0.044	0.045	0.045	0.043	0.045	0.045	0.044	0.038	0.044	0.043	0.043	0.038	0.032
2	0.045	0.044	0.044	0.044	0.045	0.042	0.045	0.045	0.043	0.040	0.045	0.045	0.042	0.041	0.031
1	0.046	0.046	0.044	0.044	0.044	0.043	0.046	0.044	0.042	0.039	0.045	0.045	0.043	0.039	0.031
0.5	0.046	0.044	0.046	0.044	0.044	0.043	0.046	0.044	0.043	0.039	0.046	0.045	0.042	0.038	0.031
0.25	0.040	0.045	0.045	0.040	0.040	com	mon long	memorv fa	ctor	0.057	0.045	0.040	0.041	0.050	0.052
							Theil	index							
T = 100	d = 0.2	<i>d</i> =	0.4		d = 0.6			<i>d</i> =	0.8				d = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.196	0.209	0.211	0.120	0.123	0.130	0.088	0.089	0.095	0.108	0.062	0.063	0.067	0.075	0.097
2	0.130	0.176	0.177	0.086	0.087	0.092	0.062	0.065	0.067	0.076	0.044	0.044	0.047	0.035	0.069
0.5	0.121	0.142	0.130	0.043	0.002	0.005	0.031	0.032	0.034	0.034	0.022	0.032	0.033	0.027	0.034
0.25	0.089	0.135	0.135	0.030	0.031	0.033	0.022	0.022	0.024	0.027	0.015	0.016	0.017	0.019	0.024
						(	correlation	coefficien	t						
T = 100	d = 0.2	<i>d</i> =	0.4		d = 0.6			<i>d</i> =	= <i>0.8</i>	r			<i>d</i> = 1.0	. <u> </u>	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.937	0.950	0.948	0.970	0.969	0.966	0.984	0.983	0.981	0.976	0.992	0.991	0.990	0.988	0.980
1	0.984	0.974	0.975	0.985	0.964	0.983	0.992	0.991	0.990	0.900	0.990	0.998	0.995	0.994	0.990
0.5	0.992	0.993	0.993	0.996	0.996	0.996	0.998	0.998	0.998	0.997	0.999	0.999	0.999	0.999	0.998
0.25	0.996	0.997	0.997	0.998	0.998	0.998	0.999	0.999	0.999	0.998	1.000	1.000	0.999	0.999	0.999
							Theil	index							
T = 500	d = 0.2	<i>d</i> =	0.4	~	d = 0.6			<i>d</i> =	0.8			<u> </u>	<i>d</i> = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.170	0.105	0.100	0.008	0.070	0.074	0.045	0.044	0.047	0.034	0.028	0.028	0.030	0.034	0.040
1	0.096	0.099	0.101	0.034	0.035	0.037	0.022	0.022	0.024	0.027	0.014	0.014	0.015	0.017	0.023
0.5	0.073	0.083	0.083	0.024	0.025	0.026	0.015	0.016	0.017	0.019	0.010	0.010	0.011	0.012	0.016
0.25	0.057	0.072	0.072	0.017	0.018	0.019	0.011	0.011	0.012	0.014	0.007	0.007	0.008	0.009	0.011
						(	correlation	coefficien	t						
T = 500	d = 0.2	<i>d</i> =	0.4	^	d = 0.6	<u> </u>	^	<i>d</i> =	- 0.8		^		d = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
2	0.945	0.930	0.934	0.995	0.990	0.988	0.990	0.990	0.995	0.994	0.990	0.999	0.999	0.997	0.998
<b>—</b>	VI. 77.77		0.777	0.770	5.775	0.774	0.770	0.770	0.770	0.771	5.777	5.777	5.777	5.777	0.770
1	0.985	0.989	0.988	0.997	0.997	0.997	0.999	0.999	0.999	0.998	1.000	1.000	1.000	0.999	0.999
<u>1</u> 0.5	0.985	0.989 0.994	0.988 0.994	0.997 0.999	0.997 0.999	0.997 0.999	0.999	0.999	0.999 0.999	0.998	1.000	1.000	1.000	0.999	0.999

Table 9: No structural break, heteroskedastic case, N=30: bias and RMSE of idiosyncratic autoregressive parameter p; Theil and correlation statistics

The Table reports Monte Carlo bias and RMSE statistics, concerning the estimation of the idiosyncratic autoregressive parameter ( $\rho$ ), and Monte Carlo *Theil index and correlation coefficient* statistics, concerning the estimation of the unobserved common long memory factor component. Results are reported for various values of the common factor fractional differencing parameter d (0.2, 0.4, 0.6, 0.8, 1), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0.2, 0.4, 0.6, 0.8), assuming  $d > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 30, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved common long memory factor and no breaks, and known fractional differencing parameter.

							Λ	I = 30							
							1-break	point case							
						au	toregressiv	e paramete	rρ						
T = 100	d = 0.2	<i>d</i> -	- 0 1	1	1-06		Di	uas d -	- 0 8		1		d = 1.0		
$(s/n)^{-1}$	u = 0.2	a = 0	a = 0.2	$\rho = 0$	a = 0.0	$\rho = 0.4$	$\rho = 0$	a = 0.2	a = 0.4	$\rho = 0.6$	$\rho = 0$	$\rho = 0.2$	u = 1.0	a = 0.6	$\rho = 0.8$
4	-0.024	-0.026	-0.031	-0.026	-0.035	-0.051	-0.025	-0.042	-0.049	-0.067	-0.036	-0.041	-0.053	-0.067	-0.084
2	-0.017	-0.026	-0.037	-0.026	-0.038	-0.048	-0.028	-0.040	-0.053	-0.066	-0.031	-0.043	-0.055	-0.067	-0.082
1	-0.021	-0.026	-0.036	-0.027	-0.040	-0.053	-0.030	-0.040	-0.047	-0.065	-0.029	-0.039	-0.053	-0.064	-0.081
0.5	-0.024	-0.022	-0.035	-0.028	-0.038	-0.047	-0.027	-0.042	-0.055	-0.065	-0.036	-0.038	-0.051	-0.069	-0.085
0.25	-0.024	-0.026	-0.035	-0.025	-0.040	-0.050	-0.033	-0.038	-0.051	-0.061	-0.027	-0.039	-0.053	-0.063	-0.083
T = 100	4-02	4-	- 0 4	1	1-06	1	oot mean s	square erro	r - 0 9		1		4-10		
I = I00	a = 0.2	a = 0	0.4	a = 0	a = 0.0	a = 0.4	a = 0	a = 0.2	0.8 = 0.4	0 = 0.6	a = 0	a = 0.2	a = 1.0	a = 0.6	a = 0.8
4	0.104	0.107	0.109	0.106	0.111	0.120	0.107	0.117	0.119	0.129	0.114	0.114	0.121	0.129	0.144
2	0.104	0.108	0.111	0.108	0.112	0.120	0.107	0.115	0.121	0.129	0.107	0.115	0.121	0.129	0.139
1	0.103	0.107	0.111	0.108	0.113	0.122	0.109	0.115	0.116	0.127	0.109	0.112	0.122	0.127	0.138
0.5	0.105	0.104	0.108	0.107	0.113	0.116	0.106	0.114	0.122	0.129	0.112	0.114	0.120	0.132	0.143
0.25	0.105	0.104	0.111	0.105	0.113	0.120	0.109	0.111	0.120	0.123	0.108	0.114	0.119	0.126	0.141
						au	toregressiv	e paramete	rρ						
T = 500	d = 0.2	d -	= 0 4		d = 0.6		bi	us d -	= 0.8				d = 1.0		
$(s/n)^{-1}$	n = 0	$\rho = \theta$	0.4	$\rho = \theta$	a = 0.0	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0$	$\rho = 0.2$	a = 1.0	$\rho = 0.6$	$\rho = 0.8$
4	-0.004	-0.004	-0.005	-0.005	-0.008	-0.010	-0.006	-0.007	-0.010	-0.013	-0.005	-0.010	-0.010	-0.012	-0.014
2	-0.004	-0.004	-0.007	-0.006	-0.007	-0.010	-0.006	-0.010	-0.010	-0.011	-0.007	-0.009	-0.010	-0.012	-0.014
1	-0.003	-0.004	-0.006	-0.005	-0.008	-0.009	-0.005	-0.009	-0.010	-0.012	-0.008	-0.007	-0.009	-0.013	-0.015
0.5	-0.003	-0.005	-0.008	-0.006	-0.008	-0.009	-0.005	-0.008	-0.010	-0.012	-0.006	-0.008	-0.009	-0.012	-0.014
0.25	-0.004	-0.006	-0.007	-0.005	-0.008	-0.010	-0.007	-0.007	-0.011	-0.014	-0.005	-0.010	-0.011	-0.012	-0.016
T - 500	d = 0.2	<i>d</i> -	- 0 1	1	1-06	1	oot mean s	square erro - d	r - 0 8		1		d = 1.0		
1 - 500	a = 0.2	a = 0	0.4	$\rho = 0$	a = 0.0	$\rho = 0.4$	$\rho = 0$	a = 0.2	0.0 = 0.4	$\rho = 0.6$	$\rho = 0$	$\rho = 0.2$	a = 1.0 a = 0.4	$\rho = 0.6$	a = 0.8
4	0.045	0.045	0.044	0.046	0.045	0.044	0.045	0.045	0.043	0.040	0.047	0.045	0.044	0.040	0.035
2	0.044	0.046	0.044	0.045	0.045	0.043	0.046	0.047	0.043	0.039	0.045	0.047	0.045	0.041	0.035
1	0.043	0.045	0.045	0.045	0.046	0.044	0.046	0.046	0.043	0.041	0.046	0.045	0.043	0.041	0.035
0.5	0.044	0.045	0.046	0.046	0.044	0.043	0.044	0.047	0.043	0.041	0.045	0.045	0.043	0.040	0.034
0.25	0.045	0.045	0.044	0.044	0.046	0.043	0.045	0.045	0.045	0.042	0.046	0.048	0.044	0.040	0.037
							2-Dreak [	ooini cuse	22.0						
						uu	bi	ias	<i>i p</i>						
T = 100	d = 0.2	<i>d</i> =	= 0.4		d = 0.6			<i>d</i> =	= 0.8				d = 1.0		,
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	-0.018	-0.024	-0.034	-0.024	-0.041	-0.050	-0.024	-0.038	-0.057	-0.062	-0.026	-0.041	-0.053	-0.065	-0.080
2	-0.021	-0.026	-0.034	-0.029	-0.037	-0.051	-0.030	-0.040	-0.044	-0.061	-0.031	-0.041	-0.048	-0.064	-0.080
0.5	-0.024	-0.023	-0.035	-0.028	-0.039	-0.040	-0.020	-0.038	-0.051	-0.003	-0.031	-0.037	-0.030	-0.003	-0.073
0.25	-0.019	-0.025	-0.030	-0.029	-0.039	-0.050	-0.032	-0.038	-0.047	-0.061	-0.031	-0.039	-0.051	-0.062	-0.077
						1	oot mean	square erro	r						
T = 100	d = 0.2	<i>d</i> =	= 0.4		d = 0.6			d =	= 0.8				d = 1.0		
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.105	0.103	0.111	0.108	0.115	0.119	0.104	0.113	0.125	0.125	0.106	0.115	0.122	0.127	0.139
2	0.103	0.109	0.110	0.100	0.112	0.119	0.108	0.110	0.113	0.122	0.108	0.114	0.119	0.126	0.13/
0.5	0.100	0.103	0.111	0.109	0,111	0,114	0.107	0.112	0.121	0.123	0.109	0.113	0.120	0.125	0.137
0.25	0.102	0.106	0.107	0.108	0.111	0.119	0.109	0.112	0.115	0.122	0.109	0.113	0.118	0.125	0.133
				-	·	au	toregressiv	e paramete	rρ		-	·	·	·	·
							bi	ias							
T = 500	d = 0.2	<i>d</i> =	= 0.4		d = 0.6			<i>d</i> =	= 0.8				d = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	-0.005	-0.006	-0.008	-0.008	-0.006	-0.010	-0.004	-0.007	-0.011	-0.011	-0.006	-0.006	-0.009	-0.013	-0.015
1	-0.005	-0.005	-0.006	-0.007	-0.006	-0.011	-0.006	-0.010	-0.012	-0.011	-0.005	-0.008	-0.008	-0.012	-0.015
0.5	-0.005	-0.005	-0.007	-0.006	-0.009	-0.009	-0.005	-0.010	-0.012	-0.013	-0.005	-0.009	-0.009	-0.011	-0.015
0.25	-0.003	-0.005	-0.008	-0.005	-0.008	-0.010	-0.005	-0.009	-0.010	-0.013	-0.005	-0.009	-0.009	-0.013	-0.015
						1	oot mean :	square erro	r						
T = 500	d = 0.2	<i>d</i> =	= 0.4		d = 0.6		~	<i>d</i> =	= 0.8		<u>^</u>		d = 1.0	a	
(s/n)-1	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.046	0.046	0.044	0.046	0.044	0.043	0.045	0.044	0.044	0.040	0.045	0.044	0.044	0.041	0.035
1	0.045	0.044	0.045	0.045	0.045	0.044	0.045	0.044	0.045	0.040	0.045	0.045	0.043	0.040	0.035
0.5	0.045	0.046	0.044	0.045	0.045	0.043	0.046	0.047	0.044	0.042	0.046	0.047	0.044	0.039	0.035
0.25	0.045	0.046	0.045	0.044	0.045	0.045	0.045	0.045	0.043	0.041	0.046	0.046	0.044	0.041	0.035

Table 10: Single and multiple break points, heteroskedastic case, N=30: bias and RMSE of idiosyncratic autoregressive parameter  $\rho$ 

 $(J_2S_1, 0.045_2, 0.045_2, 0.045_2, 0.044_2, 0.045_2, 0.045_2, 0.045_2, 0.045_2, 0.045_2, 0.045_2, 0.045_2, 0.046_2, 0.046_2, 0.046_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0.041_2, 0$ 

		<i>I</i>	,		,		Ν	<i>I=30</i>							
						con	nmon long	g memory fa	actor						
							1-break	point case							
				1			Thei	l index			1				
T = 100	d = 0.2	<i>d</i> :	= 0.4		d = 0.6			<i>d</i> :	= 0.8				d = 1.0		
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.211	0.249	0.250	0.290	0.291	0.296	0.315	0.315	0.318	0.323	0.337	0.337	0.338	0.341	0.350
1	0.170	0.221	0.222	0.273	0.273	0.270	0.303	0.303	0.307	0.310	0.331	0.332	0.332	0.334	0.339
0.5	0.129	0.196	0.196	0.256	0.255	0.257	0.296	0.296	0.296	0.297	0.320	0.327	0.327	0.328	0.329
0.25	0.119	0.191	0.191	0.252	0.253	0.253	0.294	0.294	0.294	0.295	0.326	0.326	0.326	0.326	0.327
	•						correlatio	n coefficien	nt .						
T = 100	d = 0.2	d :	= 0.4		d = 0.6			d	= 0.8				d = 1.0		
(s/n) <sup>-1</sup>	$\rho = 0$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.923	0.900	0.898	0.882	0.881	0.877	0.829	0.829	0.826	0.820	0.767	0.766	0.765	0.763	0.754
2	0.952	0.923	0.923	0.900	0.899	0.897	0.839	0.839	0.837	0.834	0.771	0.771	0.771	0.769	0.765
1	0.967	0.936	0.936	0.908	0.908	0.907	0.844	0.844	0.843	0.842	0.774	0.775	0.775	0.775	0.774
0.5	0.973	0.942	0.942	0.915	0.915	0.912	0.840	0.848	0.840	0.843	0.776	0.775	0.775	0.775	0.774
0.25	0.977	0.940	0.945	0.915	0.915	0.915	0.040 Thei	l index	0.040	0.047	0.770	0.770	0.770	0.115	0.115
T = 500	d = 0.2	d	= 0.4		d = 0.6			d :	= 0.8				d = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.180	0.176	0.179	0.316	0.316	0.318	0.323	0.324	0.324	0.326	0.327	0.327	0.328	0.329	0.332
2	0.135	0.142	0.143	0.309	0.309	0.310	0.320	0.320	0.321	0.322	0.326	0.326	0.326	0.327	0.328
1	0.103	0.119	0.120	0.305	0.305	0.306	0.318	0.318	0.319	0.319	0.325	0.325	0.325	0.326	0.326
0.5	0.082	0.106	0.106	0.303	0.303	0.303	0.317	0.317	0.317	0.318	0.325	0.325	0.325	0.325	0.325
0.25	0.069	0.098	0.098	0.302	0.302	0.302	0.317	0.317	0.317	0.317	0.324	0.324	0.324	0.325	0.325
T - 500	4-02	4.	- 0.1	1	4-06		correlatio	n coefficien			1		1-10		
1 - 300	a = 0.2	a = 0	-0.4	a = 0	a = 0.0	a = 0.4	a = 0	a = 0.2	-0.0	a = 0.6	a = 0	a = 0.2	a = 1.0	a = 0.6	a = 0.8
(3/1)	0.939	0.947	0.945	0.791	0.791	0.789	0.781	0.781	0.781	0.779	0.776	0.776	0.775	0.774	0.772
2	0.967	0.968	0.967	0.797	0.797	0.796	0.784	0.784	0.784	0.783	0.777	0.777	0.776	0.776	0.775
1	0.982	0.979	0.979	0.800	0.800	0.799	0.785	0.785	0.785	0.785	0.777	0.777	0.777	0.777	0.776
0.5	0.989	0.985	0.984	0.801	0.801	0.801	0.786	0.786	0.786	0.786	0.777	0.777	0.777	0.777	0.777
0.25	0.993	0.988	0.987	0.802	0.802	0.802	0.786	0.786	0.786	0.786	0.778	0.778	0.778	0.778	0.777
							2-break	point case							
7 100	1 0 0	,	0.4	-	1.07		Thei	l index	0.0				1 10		
I = 100	a = 0.2	a = a	= 0.4	0 - 0	d = 0.6	a = 0.4	0 - 0	a = 0.2	= 0.8	0-06	0 - 0	a = 0.2	a = 1.0	0-06	0-09
(5/11)	p = 0 0.226	p = 0 0.279	p = 0.2 0.280	p = 0 0.358	p = 0.2 0.358	p = 0.4 0.362	p - v 0.402	p = 0.2 0.402	p = 0.4 0.403	0 407	p = 0 0.447	p = 0.2 0.447	p = 0.4 0.448	p = 0.0 0.450	p = 0.8 0.453
2	0.188	0.255	0.256	0.345	0.345	0.347	0.395	0.395	0.396	0.398	0.445	0.445	0.445	0.446	0.448
1	0.165	0.242	0.242	0.338	0.338	0.339	0.391	0.391	0.392	0.393	0.443	0.443	0.443	0.444	0.445
0.5	0.152	0.235	0.235	0.334	0.334	0.334	0.389	0.389	0.390	0.390	0.442	0.442	0.443	0.443	0.443
0.25	0.144	0.231	0.231	0.332	0.332	0.332	0.388	0.388	0.388	0.389	0.442	0.442	0.442	0.442	0.442
	r			-			correlatio	n coefficien	ıt –						
T = 100	d = 0.2	<i>d</i> :	= 0.4		d = 0.6		0	<i>d</i> :	= 0.8				d = 1.0	i	
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.910	0.880	0.879	0.748	0.747	0.743	0.099	0.099	0.090	0.090	0.653	0.652	0.652	0.643	0.639
1	0.940	0.900	0.903	0.703	0.703	0.703	0.715	0.709	0.708	0.703	0.656	0.656	0.656	0.655	0.653
0.5	0.964	0.926	0.926	0.778	0.778	0.778	0.718	0.718	0.717	0.717	0.658	0.658	0.658	0.657	0.656
0.25	0.968	0.929	0.929	0.781	0.781	0.780	0.719	0.719	0.719	0.719	0.658	0.658	0.658	0.658	0.657
							Thei	l index							
T = 500	d = 0.2	d	= 0.4		<i>d</i> = 0.6			d	= 0.8				d = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = \overline{0.2}$	$\rho = \overline{\theta}$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \overline{\theta}$	$\rho = \overline{0.2}$	$\rho = \overline{0.4}$	$\rho = \overline{0.6}$	$\rho = \theta$	$\rho = \overline{0.2}$	$\rho = 0.4$	$\rho = \overline{0.6}$	$\rho = 0.8$
4	0.188	0.191	0.193	0.412	0.412	0.413	0.436	0.436	0.436	0.437	0.454	0.454	0.455	0.455	0.456
2	0.146	0.160	0.161	0.408	0.408	0.409	0.434	0.434	0.435	0.435	0.454	0.454	0.454	0.454	0.455
1	0.118	0.141	0.141	0.406	0.406	0.407	0.434	0.434	0.434	0.434	0.454	0.454	0.454	0.454	0.454
0.25	0.100	0.123	0.130	0.405	0.405	0.405	0.433	0.433	0.433	0.433	0.453	0.453	0.454	0.454	0.454
0.40	0.070	0.120	0.124	0.100	0.100	0.100	correlatio	n coefficien	0.455	0.400	0.100	0.400	0.400	0.400	0.404
T = 500	d = 0.2	d	= 0.4		d = 0.6			d	= 0.8				<i>d</i> = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.933	0.936	0.934	0.686	0.686	0.684	0.660	0.659	0.659	0.657	0.639	0.639	0.638	0.638	0.635
2	0.960	0.957	0.956	0.693	0.692	0.692	0.662	0.662	0.662	0.661	0.640	0.640	0.640	0.639	0.638
1	0.975	0.968	0.967	0.696	0.696	0.695	0.664	0.664	0.663	0.663	0.640	0.640	0.640	0.640	0.640
0.5	0.982	0.974	0.973	0.698	0.698	0.697	0.664	0.664	0.664	0.664	0.641	0.641	0.641	0.641	0.640
11 75															

 Table 11: Single and multiple break points, heteroskedastic case, N=30: Monte Carlo Theil and correlation statistics

The Table reports Monte Carlo *Theil index and correlation coefficient* statistics concerning the estimation of the unobserved common long memory factor component. Results are reported for various values of the fractional differencing parameter d (0.2, 0.4, 0.6, 0.8, 1), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0.2, 0.4, 0.6, 0.8), assuming  $d > \rho$ , and various values of the (inverse) signal to noise ratio (s/n)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 30, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved common long memory factor and known fractional differencing parameter and break points.

							N	=30							
							common b	reak proces	is .						
							1-break	point case							
<b>T</b> 100							Thei	l index							
T = 100	d = 0.2	<i>d</i> =	= 0.4	0	d = 0.6	0.4	. – 0	d =	= 0.8	0 (	0	0.2	d = 1.0	0 (	0.0
(s/n) A	p - v	p - 0	p = 0.2	p - v	p = 0.2	p = 0.4	p - v	p = 0.2	p = 0.4	p = 0.0	p - v	p = 0.2	p = 0.4	p = 0.0	p = 0.8
2	0.039	0.076	0.076	0.077	0.078	0.078	0.089	0.088	0.089	0.089	0.096	0.096	0.096	0.096	0.097
1	0.039	0.076	0.076	0.077	0.077	0.078	0.088	0.088	0.089	0.089	0.096	0.096	0.096	0.096	0.097
0.5	0.039	0.076	0.076	0.077	0.077	0.077	0.088	0.088	0.088	0.089	0.096	0.096	0.096	0.096	0.096
0.25	0.039	0.075	0.075	0.077	0.077	0.077	0.088	0.088	0.088	0.088	0.096	0.096	0.096	0.096	0.096
				-			correlatio	n coefficien	t						
T = 100	d = 0.2	<i>d</i> =	= 0.4		d = 0.6	i		<i>d</i> =	= 0.8				d = 1.0	i	
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
1	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
0.5	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
0.25	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
							Thei	l index							
$T = 5\theta\theta$	d = 0.2	<i>d</i> =	= 0.4		d = 0.6			<i>d</i> =	= 0.8				d = 1.0		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	0.019	0.038	0.038	0.091	0.091	0.091	0.094	0.095	0.095	0.095	0.096	0.096	0.096	0.096	0.096
2	0.018	0.038	0.038	0.091	0.091	0.091	0.095	0.095	0.095	0.095	0.096	0.096	0.096	0.096	0.096
1	0.018	0.038	0.038	0.091	0.091	0.091	0.095	0.095	0.095	0.095	0.096	0.096	0.096	0.096	0.096
0.5	0.018	0.038	0.038	0.091	0.091	0.091	0.095	0.093	0.093	0.095	0.096	0.096	0.096	0.096	0.096
0.25	0.010	0.050	0.020	0.071	0.071	0.071	correlatio	n coefficien	t	0.075	0.070	0.070	0.070	0.070	0.070
T = 500	d = 0.2	<i>d</i> =	= 0.4		d = 0.6			d =	= 0.8				d = 1.0		
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
4	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
2	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
1	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
0.5	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
0.25	1.000	1.000	1.000	1.000	1.000	1.000	2 hugak	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
							2-Dieun	poini cuse							
							Thei	l index							
T = 100	d = 0.2	<i>d</i> =	= 0.4		<i>d</i> = 0.6		Thei	l index d =	= 0.8				d = 1.0		
T = 100 (s/n) <sup>-1</sup>	$\frac{d=0.2}{\rho=0}$	$d = \rho = \theta$	$= 0.4$ $\rho = 0.2$	$\rho = 0$	$d = 0.6$ $\rho = 0.2$	$\rho = 0.4$	Thei ρ = 0	$\frac{l \text{ index}}{\rho = 0.2}$	$= 0.8$ $\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$d = 1.0$ $\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$
$T = 100$ $(s/n)^{-1}$ $4$	d = 0.2 $\rho = 0$ 0.054	$d = \rho = \theta$ 0.101	= <b>0.4</b> <b>ρ</b> = <b>0.2</b> 0.101	$\rho = \theta$ 0.108	d = 0.6 $\rho = 0.2$ 0.108	<i>ρ</i> = <i>θ.4</i> 0.109	p = 0 $0.122$	$\frac{l \text{ index}}{d} = \frac{d}{\rho = 0.2}$ 0.122	<b><i>ρ</i> = 0.8</b> <b><i>ρ</i> = 0.4</b> 0.122	<b>ρ = 0.6</b> 0.123	<b>ρ</b> = <b>θ</b> 0.134	<i>ρ</i> = <i>θ.2</i> 0.134	d = 1.0 $\rho = 0.4$ 0.134	<b>ρ = 0.6</b> 0.134	<b>ρ = 0.8</b> 0.135
	d = 0.2 $\rho = 0$ 0.054 0.054	<i>d</i> = <i>ρ</i> = <i>θ</i> 0.101 0.101	$= 0.4$ $\rho = 0.2$ 0.101 0.101	<i>ρ</i> = <i>θ</i> 0.108 0.108	<i>d</i> = 0.6 <i>ρ</i> = 0.2 0.108 0.108	<i>ρ</i> = 0.4 0.109 0.109	<i>Thei ρ</i> = 0 0.122 0.122	<i>l index</i> <i>d</i> = <i>p</i> = 0.2 0.122 0.122	<b>= 0.8</b> <b>ρ = 0.4</b> 0.122 0.122	<i>ρ</i> = 0.6 0.123 0.122	<i>ρ</i> = 0 0.134 0.134	<i>ρ</i> = 0.2 0.134 0.134	d = 1.0 $\rho = 0.4$ 0.134 0.134	<i>ρ</i> = 0.6 0.134 0.134	<i>ρ</i> = 0.8 0.135 0.135
$T = 100$ $(s/n)^{-1}$ $4$ $2$ $1$	d = 0.2 p = 0 0.054 0.054 0.053	$d = \rho = 0$ 0.101 0.101 0.101	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101	$\rho = 0$ 0.108 0.108 0.108	d = 0.6 $\rho = 0.2$ 0.108 0.108 0.108	$\rho = 0.4$ 0.109 0.109 0.108	<i>Thei</i> $\rho = 0$ 0.122 0.122 0.122 0.122	$ \frac{d}{\rho = 0.2} $ 0.122 0.122 0.122 0.122		$\rho = 0.6$ 0.123 0.122 0.122	p = 0 0.134 0.134 0.134	$\rho = 0.2$ 0.134 0.134 0.134	d = 1.0 $\rho = 0.4$ 0.134 0.134 0.134	$\rho = 0.6$ 0.134 0.134 0.134	$\rho = 0.8$ 0.135 0.135 0.134
T = 100 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25	$d = 0.2$ $\rho = 0$ 0.054 0.054 0.053 0.053 0.053	$d = \frac{\rho = \theta}{0.101}$ 0.101 0.101 0.100 0.100	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101 0.101	$\rho = 0$ 0.108 0.108 0.108 0.108 0.108	d = 0.6 $\rho = 0.2$ 0.108 0.108 0.108 0.108	$\rho = 0.4$ 0.109 0.109 0.108 0.108	<i>Thei</i> p = 0 0.122 0.122 0.122 0.122 0.122	$\frac{d}{\rho = 0.2}$ 0.122 0.122 0.122 0.122 0.122 0.122 0.122		<i>ρ</i> = 0.6 0.123 0.122 0.122 0.122 0.122	<i>ρ</i> = <i>θ</i> 0.134 0.134 0.134 0.134	$\rho = 0.2$ 0.134 0.134 0.134 0.134 0.134	$d = 1.0$ $\rho = 0.4$ 0.134 0.134 0.134 0.134 0.134	$\rho = 0.6$ 0.134 0.134 0.134 0.134 0.134	$\rho = 0.8$ 0.135 0.135 0.134 0.134
T = 100 (s/n) <sup>-1</sup> 4 2 1 0.5 0.25	$\begin{array}{c} d = 0.2 \\ p = 0 \\ 0.054 \\ 0.053 \\ 0.053 \\ 0.053 \end{array}$	<i>d</i> = <i>ρ</i> = <i>θ</i> 0.101 0.101 0.101 0.100 0.100	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101 0.100	<i>ρ</i> = <i>θ</i> 0.108 0.108 0.108 0.108 0.108	<i>d</i> = 0.6 <i>ρ</i> = 0.2 0.108 0.108 0.108 0.108 0.108		<i>Thei</i> $\rho = 0$ 0.122 0.122 0.122 0.122 0.122 0.122	$ \begin{array}{r}     d = \\     \hline \rho = 0.2 \\     0.122 \\     0.122 \\     0.122 \\     0.122 \\     0.122 \\     0.122 \\     0.122 \\   \end{array} $	= 0.8 $p = 0.4$ 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122	<b>ρ</b> = <b>0.6</b> 0.123 0.122 0.122 0.122 0.122	<b>ρ</b> = <b>θ</b> 0.134 0.134 0.134 0.134 0.134	<i>ρ</i> = 0.2 0.134 0.134 0.134 0.134 0.134	$d = 1.0$ $\rho = 0.4$ 0.134 0.134 0.134 0.134 0.134	<i>ρ</i> = 0.6 0.134 0.134 0.134 0.134 0.134	<i>ρ</i> = 0.8 0.135 0.135 0.134 0.134 0.134
$     \begin{array}{r}       T = 100 \\       (s/n)^{-1} \\       4 \\       2 \\       1 \\       0.5 \\       0.25 \\       \hline       T = 100     \end{array} $	d = 0.2 $\rho = 0$ 0.054 0.054 0.053 0.053 0.053 0.053 0.053 0.053	$d = \rho = 0$ 0.101 0.101 0.101 0.100 0.100 0.100	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101 0.101 0.100 $= 0.4$	<b>ρ</b> = <b>θ</b> 0.108 0.108 0.108 0.108 0.108	$d = 0.6$ $\rho = 0.2$ 0.108 0.108 0.108 0.108 0.108 0.108 0.108	p = 0.4 0.109 0.109 0.108 0.108 0.108	$\rho = 0$ 0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122	<i>l index</i> <i>d</i> = <i>p</i> = 0.2 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122	= 0.8 $p = 0.4$ 0.122 0.122 0.122 0.122 0.122 0.122 0.122 t = 0.8	<i>p</i> = 0.6 0.123 0.122 0.122 0.122 0.122	<b>ρ</b> = <b>θ</b> 0.134 0.134 0.134 0.134 0.134	p = 0.2           0.134           0.134           0.134           0.134	d = 1.0 $p = 0.4$ 0.134 0.134 0.134 0.134 0.134 0.134	<i>ρ</i> = 0.6 0.134 0.134 0.134 0.134 0.134	$\rho = 0.8$ 0.135 0.135 0.134 0.134 0.134
$     \begin{array}{r}       T = 100 \\       (s/n)^{-1} \\       4 \\       2 \\       1 \\       0.5 \\       0.25 \\       \hline       T = 100 \\       (s/n)^{-1}     \end{array} $	d = 0.2 $\rho = 0$ 0.054 0.053 0.053 0.053 0.053 d = 0.2 $\rho = 0$	$d = \rho = \theta$ 0.101 0.101 0.101 0.100 0.100 $d = \rho = \theta$	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101 0.100 $= 0.4$ $\rho = 0.2$	$\rho = \theta$ 0.108 0.108 0.108 0.108 0.108 $\rho = \theta$	$d = 0.6$ $\rho = 0.2$ 0.108 0.108 0.108 0.108 0.108 0.108 0.108 d = 0.6 $\rho = 0.2$	$\rho = 0.4$ 0.109 0.109 0.108 0.108 0.108 $\rho = 0.4$	Their $\rho = \theta$ 0.122 0.122 0.122 0.122 0.122 0.122 correlation $\rho = \theta$	$\begin{array}{c} d = \\ \hline p = 0.2 \\ \hline 0.122 \\ \hline$	= 0.8 $p = 0.4$ 0.122 0.122 0.122 0.122 0.122 0.122 0.122 t $= 0.8$ $p = 0.4$	$\rho = 0.6$ 0.123 0.122 0.122 0.122 0.122 0.122 0.122	$\rho = 0$ 0.134 0.134 0.134 0.134 0.134 0.134 $\rho = 0$	$\rho = 0.2$ 0.134 0.134 0.134 0.134 0.134 0.134	$d = 1.0$ $\rho = 0.4$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 $d = 1.0$ $\rho = 0.4$	$\rho = 0.6$ 0.134 0.134 0.134 0.134 0.134 0.134	$\rho = 0.8$ 0.135 0.135 0.134 0.134 0.134 0.134
$     \begin{array}{r}       T = 100 \\       (s/n)^{-1} \\       4 \\       2 \\       1 \\       0.5 \\       0.25 \\       \hline       T = 100 \\       (s/n)^{-1} \\       4     \end{array} $	d = 0.2 $\rho = 0$ 0.054 0.053 0.053 0.053 0.053 d = 0.2 $\rho = 0$ 0.994	$d = \frac{\rho = \theta}{0.101}$ 0.101 0.101 0.100 0.100 0.100 $d = \frac{\rho = \theta}{0.981}$	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101 0.100 $= 0.4$ $\rho = 0.2$ 0.981	$\rho = \theta$ 0.108 0.108 0.108 0.108 0.108 0.108 0.108 0.108 $\rho = \theta$ 0.956	$d = 0.6$ $\rho = 0.2$ 0.108 0.108 0.108 0.108 0.108 0.108 $d = 0.6$ $\rho = 0.2$ 0.956	$\rho = 0.4$ 0.109 0.109 0.108 0.108 0.108 $\rho = 0.4$ 0.956	$     \begin{array}{r}       Thei         \\             \rho = 0 \\             0.122 \\             0.122 \\             0.122 \\             0.122 \\             0.122 \\             0.122 \\             correlation         \\             \rho = 0 \\             0.947 \\         \end{array}     $	$findex = \frac{1}{p = 0.2}$ 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.12 0.1	= 0.8 $p = 0.4$ 0.122 0.122 0.122 0.122 0.122 0.122 t $= 0.8$ $p = 0.4$ 0.947	$\rho = 0.6$ 0.123 0.122 0.122 0.122 0.122 0.122 0.122 0.122	<b>ρ</b> = <b>θ</b> 0.134 0.134 0.134 0.134 0.134 <b>ρ</b> = <b>θ</b> 0.936	$\rho = 0.2$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134	$d = 1.0$ $\rho = 0.4$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134	p = 0.6 0.134 0.134 0.134 0.134 0.134 0.134 p = 0.6 0.935	$\rho = 0.8$ 0.135 0.135 0.134 0.134 0.134 0.134 0.134 0.134
	d = 0.2 p = 0 0.054 0.053 0.053 0.053 0.053 d = 0.2 p = 0 0.994 0.994	$d = \frac{\rho = \theta}{0.101}$ 0.101 0.101 0.100 0.100 0.100 $d = \frac{\rho = \theta}{0.981}$ 0.981	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101 0.100 $= 0.4$ $\rho = 0.2$ 0.981 0.981	ρ = θ           0.108           0.108           0.108           0.108           0.108           0.108           0.108           0.108           0.108	$d = 0.6$ $\rho = 0.2$ 0.108 0.108 0.108 0.108 0.108 0.108 $d = 0.6$ $\rho = 0.2$ 0.956 0.956	$\rho = 0.4$ 0.109 0.109 0.108 0.108 0.108 $\rho = 0.4$ 0.956 0.956	p = 0           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.124 $p = 0$ 0.947           0.947	$findex = \frac{1}{p = 0.2}$ 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.0122 0.0122 0.012 0.012 0.012 0.012 0.012 0.012 0.012 0.01 0.01	= 0.8 $p = 0.4$ 0.122 0.122 0.122 0.122 0.122 0.122 t $= 0.8$ $p = 0.4$ 0.947 0.947	<i>ρ</i> = 0.6 0.123 0.122 0.122 0.122 0.122 0.122 <i>φ</i> = 0.6 0.946 0.947	<b>ρ = 0</b> 0.134 0.134 0.134 0.134 0.134 0.134 <b>ρ = 0</b> 0.936 0.935	$\rho = 0.2$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134	$d = 1.0$ $\rho = 0.4$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134	p = 0.6 0.134 0.134 0.134 0.134 0.134 0.134 p = 0.6 0.935 0.935	$\rho = 0.8$ 0.135 0.135 0.134 0.134 0.134 0.134 0.134 0.134 0.134
$     \begin{array}{r} T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline \\ T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 1 \\ \hline \\ \end{array} $	d = 0.2 $\rho = 0$ 0.054 0.053 0.053 0.053 0.053 d = 0.2 $\rho = 0$ 0.994 0.994 0.994	$d = \frac{\rho = 0}{0.101}$ 0.101 0.101 0.100 0.100 0.100 0.100 0.100 0.981 0.981 0.981 0.981	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101 0.100 $= 0.4$ $\rho = 0.2$ 0.981 0.981 0.981	$\rho = \theta$ 0.108 0.108 0.108 0.108 0.108 0.108 0.108 $\rho = \theta$ 0.956 0.956 0.956	$d = 0.6$ $\rho = 0.2$ 0.108 0.108 0.108 0.108 0.108 $d = 0.6$ $\rho = 0.2$ 0.956 0.956 0.956	$\rho = 0.4$ 0.109 0.109 0.108 0.108 0.108 $\rho = 0.4$ 0.956 0.956 0.956	$\rho = 0$ 0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.947           0.947	$findex$ $d = \frac{1}{\rho = 0.2}$ 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 0.124 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$     \begin{array}{r} T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline \end{array} $	d = 0.2 $\rho = 0$ 0.054 0.053 0.053 0.053 0.053 d = 0.2 $\rho = 0$ 0.994 0.994 0.994 0.994	$d = \frac{\rho = 0}{0.101}$ 0.101 0.101 0.100 0.100 0.100 0.100 0.100 0.981 0.981 0.981 0.981	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.100 $= 0.4$ $\rho = 0.2$ 0.981 0.981 0.981 0.981	$\rho = \theta$ 0.108 0.108 0.108 0.108 0.108 0.108 0.108 0.108 0.956 0.956 0.956 0.956 0.956	d = 0.6 $\rho = 0.2$ 0.108 0.108 0.108 0.108 d = 0.6 $\rho = 0.2$ 0.956 0.956 0.956 0.956	$\rho = 0.4$ 0.109 0.109 0.108 0.108 0.108 $\rho = 0.4$ 0.956 0.956 0.956 0.956	$\rho = 0$ 0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.124           0.125           0.126           0.127           0.947           0.947           0.947           0.947	$\begin{array}{c} l \text{ index} \\ \hline d = \\ \hline \rho = 0.2 \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.122 \\ \hline n \text{ coefficien} \\ \hline d = \\ \hline \rho = 0.2 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.94$	= 0.8 $p = 0.4$ 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.12 0.1	$\rho = 0.6$ 0.123 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122	p = 0 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.935 0.935 0.935 0.935	$\rho = 0.2$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.935 0.935 0.935 0.935	$d = 1.0$ $\rho = 0.4$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.935 0.935 0.935 0.935 0.935 0.935	<i>ρ</i> = 0.6 0.134 0.134 0.134 0.134 0.134 0.134 0.134 <i>ρ</i> = 0.6 0.935 0.935 0.935	$\rho = 0.8$ 0.135 0.135 0.134 0.134 0.134 0.134 $\rho = 0.8$ 0.935 0.935 0.935 0.935
$     \begin{array}{r} T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline \\ T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline \end{array} $	d = 0.2 $\rho = 0$ 0.054 0.053 0.053 0.053 0.053 d = 0.2 $\rho = 0$ 0.994 0.994 0.994	$d = \frac{\rho = \theta}{0.101}$ 0.101 0.101 0.100 0.100 0.100 0.100 0.100 0.981 0.981 0.981 0.981	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101 0.100 $= 0.4$ $\rho = 0.2$ 0.981 0.981 0.981 0.981	$\rho = 0$ 0.108 0.108 0.108 0.108 0.108 0.108 0.108 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 0.956 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0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.124           0.125           0.126           0.127           0.128           0.129           0.120           0.120           0.121           0.122           0.122           0.122           0.124           0.947           0.947           0.947           0.947           0.947	$\begin{array}{c} l \text{ index} \\ \hline d = \\ \hline \rho = 0.2 \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.122 \\ \hline 0.122 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 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\\ 0.935 \\ 0.935 \\ 0.935 \\ 0.935 \\ 0.935 \\ 0.935 \\ 0.935 \\ 0.935 \end{array}$	$d = 1.0$ $\rho = 0.4$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.935 0.935 0.935 0.935 0.935 0.935 0.936	<i>ρ</i> = 0.6 0.134 0.134 0.134 0.134 0.134 0.134 0.134 <i>ρ</i> = 0.6 0.935 0.935 0.935 0.935	$\rho = 0.8$ 0.135 0.135 0.134 0.134 0.134 0.134 $\rho = 0.8$ 0.935 0.935 0.935 0.935
$     \begin{array}{r} T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 500 \\ \hline \end{array} $	d = 0.2 $\rho = 0$ 0.054 0.053 0.053 0.053 0.053 d = 0.2 $\rho = 0$ 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 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0000000000000000000000000000	$\rho = 0.4$ 0.109 0.109 0.108 0.108 0.108 0.108 $\rho = 0.4$ 0.956 0.956 0.956 0.956 0.956	Thei $p = 0$ 0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.947           0.947           0.947           0.947           Thei	$\begin{array}{c} \text{I index} \\ \hline \textbf{d} = \\ \hline \textbf{\rho} = \textbf{0.2} \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.122 \\ 0.127 \\ 0.947 \\ \textbf{d} = \\ \hline \textbf{\rho} = \textbf{0.2} \\ 0.947 \\ 0.947 \\ 0.947 \\ 0.947 \\ 1 \text{index} \\ \textbf{d} = \\ \hline $	= 0.8 $p = 0.4$ 0.122 0.122 0.122 0.122 0.122 0.122 t $= 0.8$ $p = 0.4$ 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 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$     \begin{array}{r} T = 100 \\ (s/n)^{-l} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline \\ T = 100 \\ (s/n)^{-l} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline \\ 0.5 \\ 0.25 \\ \hline \\ T = 500 \\ (s/n)^{-l} \end{array} $	d = 0.2 $\rho = 0$ 0.054 0.053 0.053 0.053 0.053 d = 0.2 $\rho = 0$ 0.994 0.994 0.994 0.994 0.994 0.994	$d = \frac{\rho = \theta}{0.101}$ 0.101 0.101 0.100 0.100 0.100 0.100 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 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0.4$	$\rho = 0.6$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.935 0.935 0.935 0.935 0.935 0.935 0.935	$\rho = 0.8$ 0.135 0.135 0.134 0.134 0.134 0.134 0.134 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935
$     \begin{array}{r} T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 500 \\ (s/n)^{-1} \\ 4 \\ \end{array} $	$\begin{array}{c} d=0.2\\ \rho=0\\ 0.054\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.094\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ \end{array}$	$d = \frac{\rho = \theta}{0.101}$ 0.101 0.101 0.100 0.100 0.100 0.100 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 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$     \begin{array}{r} T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline \\ T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline \\ T = 500 \\ (s/n)^{-1} \\ 4 \\ 2 \\ \hline \end{array} $	$\begin{array}{c} d=0.2\\ \rho=0\\ 0.054\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.094\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.032\\ 0.031\\ \end{array}$	$d = \frac{\rho = \theta}{0.101}$ 0.101 0.101 0.100 0.100 0.100 0.100 0.100 0.981 0.981 0.981 0.981 0.981 0.981 d = \frac{\rho = \theta}{0.055} 0.054	$= 0.4$ $\rho = 0.2$ 0.101 0.101 0.101 0.101 0.100 $= 0.4$ $\rho = 0.2$ 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 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    0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.122           0.947           0.947           0.947           0.947           0.947           0.947           0.947           0.943           0.134           0.134	$\begin{array}{c} lindex\\ \hline d = \\ \hline \rho = 0.2\\ 0.122\\ 0.122\\ 0.122\\ 0.122\\ 0.122\\ 0.122\\ \hline 0.927\\ 0.947\\ 0.947\\ 0.947\\ 0.947\\ 0.947\\ 1 index\\ \hline d = \\ \hline \rho = 0.2\\ 0.134\\ 0.134\\ \end{array}$	= 0.8 $p = 0.4$ 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.124 0.124 0.134 0.134	$\rho = 0.6$ 0.123 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.122 0.124 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 0.947 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0.94		$\rho = 0.2$ 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.134 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935 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$\begin{array}{c} T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline\\ T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline\\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 1\\ \hline\\ 1\\ 1\\ \end{array}$	$\begin{array}{c} d=0.2\\ \rho=0\\ 0.054\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.094\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 0.003\\ 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$\begin{array}{c} T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline\\ T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline\\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline\\ 0.5\\ 0.25\\ \hline\end{array}$	$\begin{array}{c} d=0.2\\ \rho=0\\ 0.054\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.093\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 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$     \begin{array}{r} T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 500 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 500 \\ \hline T = 500 \\ \hline T = 500 \\ \hline \end{array} $	d = 0.2 $\rho = 0$ 0.054 0.053 0.053 0.053 0.053 0.053 0.053 0.094 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.031 0.031 0.031 0.031 0.031	$d = \frac{\rho = \theta}{0.101}$ 0.101 0.101 0.100 0.100 0.100 0.100 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 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$     \begin{array}{r} T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 100 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 500 \\ (s/n)^{-1} \\ 4 \\ 2 \\ 1 \\ 0.5 \\ 0.25 \\ \hline T = 500 \\ (s/n)^{-1} \\ 5 \\ 0.25 \\ \hline T = 500 \\ (s/n)^{-1} \\ $	d = 0.2 $\rho = 0$ 0.054 0.053 0.053 0.053 0.053 0.053 0.093 d = 0.2 $\rho = 0$ 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.032 $\rho = 0$ 0.031 0.031 0.031 0.031 0.031	$d = \frac{\rho = \theta}{\rho = 0}$ 0.101 0.101 0.101 0.100 0.100 0.100 0.100 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 0.981 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$\begin{array}{c} T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 4\\ \hline \\ 0.5\\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ \hline \\ 0.5\\ 0.25\\ \hline \\ \end{array}$	$\begin{array}{c} d=0.2\\ \rho=0\\ 0.054\\ 0.054\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.094\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 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$\begin{array}{c} T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ \hline \end{array}$	$\begin{array}{c} d=0.2\\ \rho=0\\ 0.054\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.094\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 0.031\\ 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$\begin{array}{c} T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 1\\ 1\\ \hline \\ 1\\ 1\\ \hline \end{array}$	$\begin{array}{c} d=0.2\\ \rho=0\\ 0.054\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.093\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 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$\begin{array}{c} T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 100\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ \hline \\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ \hline \\ 0.25\\ \hline \\ T = 500\\ (s/n)^{-1}\\ 4\\ 2\\ 1\\ 0.5\\ \hline \end{array}$	$\begin{array}{c} d=0.2\\ \rho=0\\ 0.054\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.053\\ 0.093\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.994\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 0.997\\ 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 Table 12: Single and multiple break points, heterokedastic case, N=30: Monte Carlo Theil and correlation statistics.

The Table reports Monte Carlo *Theil index and correlation coefficient* statistics concerning the estimation of the unobserved common break process component. Results are reported for various values of the fractional differencing parameter d (0.2, 0.4, 0.6, 0.8, 1), various values of the idiosyncratic autoregressive parameter p (0, 0.2, 0.4, 0.6, 0.8), assuming d > p, and various values of the (inverse) signal to noise ratio (s/n)<sup>-1</sup> (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 30, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved common long memory factor and known fractional differencing parameter and break points.

Table 13:	Single and	multiple b	reak points,	heterosk	edastic case	: Monte Ca	rlo correla	ition coeffic	ent statisti	cs.						
						con	nmon long	g memory fo	ictor							
T = 100	1-02	d = 0.2 $d = 0.4$ $d = 0.6$ $d = 0.8$ $d = 1.0$														
I = 100	a = 0.2	u = 0.4		a = 0.6			$u = 0.\delta$				$\begin{array}{c c} u = 1.0 \\ \hline \end{array}$					
(s/n)	p - v	p - v	p = 0.2	p - 0	p = 0.2	p = 0.4	p - v	p = 0.2	p = 0.4	p = 0.0	p - v	p = 0.2	p = 0.4	p = 0.0	p = 0.0	
4	0.845	0.783	0.868	0.855	0.0017	0.830	0.910	0.913	0.904	0.000	0.934	0.933	0.947	0.934	0.895	
1	0.043	0.929	0.000	0.915	0.917	0.950	0.976	0.975	0.973	0.965	0.978	0.987	0.986	0.982	0.971	
0.5	0.953	0.963	0.962	0.977	0.977	0.974	0.988	0.987	0.986	0.982	0.994	0.994	0.993	0.991	0.985	
0.25	0.976	0.981	0.980	0.989	0.988	0.987	0.994	0.994	0.993	0.991	0.997	0.997	0.996	0.995	0.993	
correlation coefficient N=10																
T = 100	d = 0.2	<i>d</i> =	= 0.4		d = 0.6			d =	= 0.8				d = 1.0			
(s/n) <sup>-1</sup>	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$	
4	0.852	0.884	0.880	0.971	0.970	0.966	0.987	0.987	0.985	0.981	0.995	0.995	0.994	0.992	0.986	
2	0.917	0.936	0.934	0.985	0.985	0.982	0.994	0.993	0.992	0.990	0.997	0.997	0.997	0.996	0.993	
1	0.956	0.967	0.965	0.992	0.992	0.991	0.997	0.997	0.996	0.995	0.999	0.999	0.999	0.998	0.997	
0.5	0.977	0.983	0.982	0.996	0.996	0.996	0.998	0.998	0.998	0.998	0.999	0.999	0.999	0.999	0.998	
0.25	0.988	0.991	0.991	0.998	0.998	0.998	0.999	0.999	0.999	0.999	1.000	1.000	1.000	1.000	0.999	
$\frac{1}{1-0.2} = \frac{1}{1-0.2} = \frac{1}{1-0.4} = $																
T = 100	d = 0.2	<i>d</i> =	= 0.4		d = 0.6			<i>d</i> =	= 0.8	0 - (		0.2	d = 1.0	0 /		
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$	
2	0.894	0.917	0.914	0.980	0.979	0.970	0.992	0.991	0.990	0.987	0.997	0.997	0.990	0.995	0.991	
2	0.945	0.930	0.934	0.990	0.989	0.988	0.990	0.990	0.993	0.993	0.998	0.998	0.998	0.997	0.990	
0.5	0.970	0.977	0.970	0.993	0.995	0.994	0.998	0.998	0.998	0.997	1.000	1.000	1.000	0.999	0.998	
0.25	0.992	0.994	0.994	0.999	0.999	0.999	1.000	0.999	0.999	0.999	1.000	1.000	1.000	1.000	0.999	
0120						corr	elation co	efficient N	1 = 50							
T = 100	d = 0.2	d =	= 0.4		d = 0.6			d =	= 0.8				d = 1.0			
$(s/n)^{-1}$	$\rho = 0$	$\rho = 0$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$	
4	0.964	0.973	0.972	0.994	0.994	0.993	0.997	0.997	0.997	0.996	0.999	0.999	0.999	0.998	0.997	
2	0.982	0.986	0.986	0.997	0.997	0.996	0.999	0.999	0.999	0.998	1.000	1.000	0.999	0.999	0.999	
1	0.991	0.993	0.993	0.998	0.998	0.998	0.999	0.999	0.999	0.999	1.000	1.000	1.000	1.000	0.999	
0.5	0.995	0.997	0.996	0.999	0.999	0.999	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
0.25	0.998	0.998	0.998	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
	1	1				cor	relation co	oefficient 1	V = 5							
T = 500	d = 0.2	<i>d</i> =	= 0.4		d = 0.6			<i>d</i> =	= 0.8				d = 1.0			
(s/n)-1	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$	
4	0.756	0.802	0.796	0.945	0.943	0.936	0.976	0.975	0.972	0.964	0.990	0.990	0.988	0.985	0.974	
1	0.855	0.884	0.001	0.971	0.970	0.900	0.988	0.987	0.985	0.981	0.993	0.995	0.994	0.992	0.987	
0.5	0.918	0.957	0.955	0.985	0.985	0.985	0.994	0.994	0.995	0.990	0.998	0.997	0.997	0.990	0.993	
0.25	0.978	0.983	0.982	0.996	0.996	0.996	0.998	0.998	0.998	0.998	0.999	0.999	0.999	0.999	0.998	
0.25	0.770	0.705	0.702	0.770	0.770	corr	elation co	efficient N	I = 10	0.770	0.777	0.777	0.777	0.777	0.770	
T = 500	d = 0.2	<i>d</i> =	d = 0.4		d = 0.6			d = 0.8				<i>d</i> = 1.0				
$(s/n)^{-1}$	$\rho = \theta$	$\rho = 0$	$\rho = 0.2$	$\rho = 0$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$	
4	0.852	0.884	0.880	0.971	0.970	0.966	0.987	0.987	0.985	0.981	0.995	0.995	0.994	0.992	0.987	
2	0.918	0.937	0.935	0.985	0.985	0.982	0.994	0.993	0.993	0.990	0.998	0.997	0.997	0.996	0.993	
1	0.956	0.967	0.966	0.992	0.992	0.991	0.997	0.997	0.996	0.995	0.999	0.999	0.999	0.998	0.997	
0.5	0.977	0.983	0.982	0.996	0.996	0.996	0.998	0.998	0.998	0.998	0.999	0.999	0.999	0.999	0.998	
0.25	0.988	0.991	0.991	0.998	0.998	0.998	0.999	0.999	0.999	0.999	1.000	1.000	1.000	1.000	0.999	
		-				corr	elation co	efficient N	<u>r=15</u>							
T = 500	d = 0.2	<i>d</i> =	= 0.4		d = 0.6			d =	= 0.8	0 /		0.2	d = 1.0	0 /		
(s/n) <sup>-1</sup>	$\rho = \eta$	p = 0	$\rho = 0.2$	p = 0	p = 0.2	p = 0.4	$\rho = 0$	p = 0.2	p = 0.4	p = 0.6	p = 0	p = 0.2	p = 0.4	p = 0.0	$\rho = 0.8$	
4	0.894	0.917	0.915	0.980	0.980	0.977	0.992	0.991	0.990	0.987	0.997	0.996	0.996	0.995	0.991	
2	0.943	0.950	0.954	0.990	0.990	0.900	0.990	0.990	0.995	0.994	0.990	0.998	0.998	0.997	0.993	
05	0.985	0.988	0.988	0.998	0.997	0.997	0.999	0.999	0.999	0.998	1.000	1 000	1 000	0.999	0.999	
0.25	0.992	0.994	0,994	0.999	0.999	0.999	1,000	0.999	0,999	0.999	1.000	1.000	1.000	1.000	0.999	
						corr	elation co	efficient N	= 50			-1000		1.000		
T = 500	d = 0.2	<i>d</i> =	= 0.4		d = 0.6	2011		d =	d = 0.8 $d = 1.0$							
$(s/n)^{-1}$	$\rho = \theta$	$\rho = \theta$	$\rho = 0.2$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = \theta$	$\rho = 0.2$	$\rho = 0.4$	$\rho = 0.6$	$\rho = 0.8$	
4	0.964	0.973	0.972	0.994	0.994	0.993	0.997	0.997	0.997	0.996	0.999	0.999	0.999	0.999	0.997	
2	0.982	0.986	0.986	0.997	0.997	0.996	0.999	0.999	0.998	0.998	1.000	1.000	0.999	0.999	0.999	
1	0.991	0.993	0.993	0.998	0.998	0.998	0.999	0.999	0.999	0.999	1.000	1.000	1.000	1.000	0.999	
0.5	0.995	0.997	0.996	0.999	0.999	0.999	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
0.25	0.998	0.998	0.998	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	

Table 13: Single and multiple break points, heteroskedastic case: Monte Carlo correlation coefficient statistics.

The Table reports Monte Carlo *correlation coefficients* between the actual and estimated common long memory factor. Results are reported for various values of the fractional differencing parameter d (0, 2, 0, 4, 0, 6, 0, 8, 1), various values of the idiosyncratic autoregressive parameter  $\rho$  (0, 0, 2, 0, 4, 0, 6, 0, 8), assuming  $d > \rho$ , and various values of the (inverse) signal to noise ratio  $(s/n)^{-1}$  (4, 2, 1, 05, 0.25). The sample size T is 100 and 500 observations, the number of cross-sectional units N is 5, 10, 15, 50, and the number of replications for each case is 2,000. The experiment refers to the case of unobserved common long memory factor and no breaks.